

Distributed Frequency and Voltage Control of Islanded Microgrids

John W. Simpson-Porco, Florian Dorfler and Francesco Bullo



Center for Control, Dynamical Systems
& Computation

University of California, Santa Barbara



Pacific Northwest National Laboratory

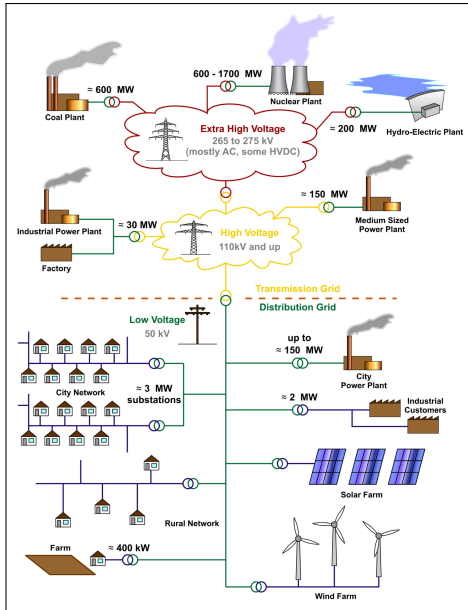
March 23, 2015

Electricity & The Power Grid



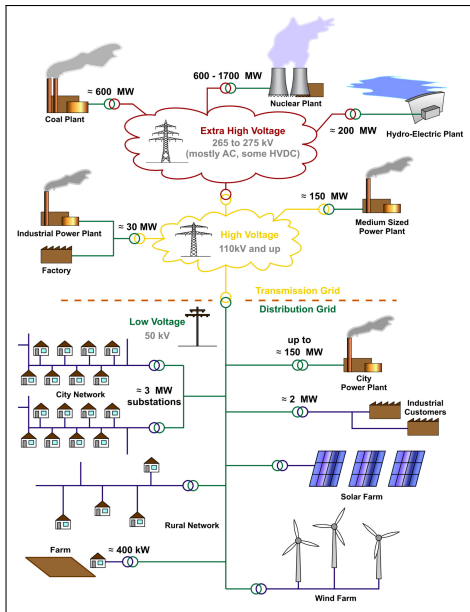
- **Electricity** is the foundation of technological civilization
- **Hierarchical** grid: generate/transmit/consume
- **Challenges:** multi-scale, nonlinear, & complex

Electricity & The Power Grid



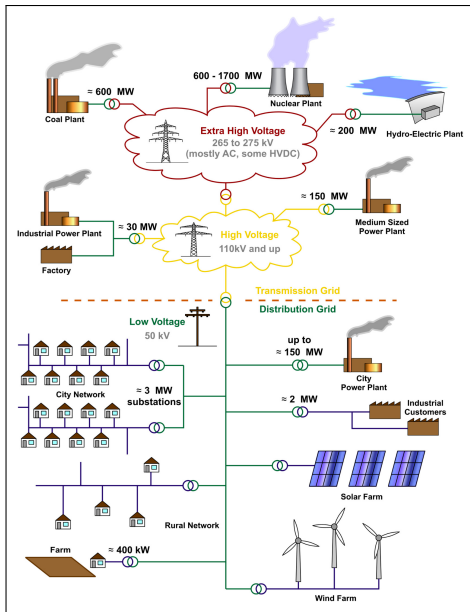
- **Electricity** is the foundation of technological civilization
- **Hierarchical** grid: generate/transmit/consume
- **Challenges:** multi-scale, nonlinear, & complex

Electricity & The Power Grid



- **Electricity** is the foundation of technological civilization
- **Hierarchical** grid: generate/transmit/consume
- **Challenges:** multi-scale, nonlinear, & complex

Electricity & The Power Grid

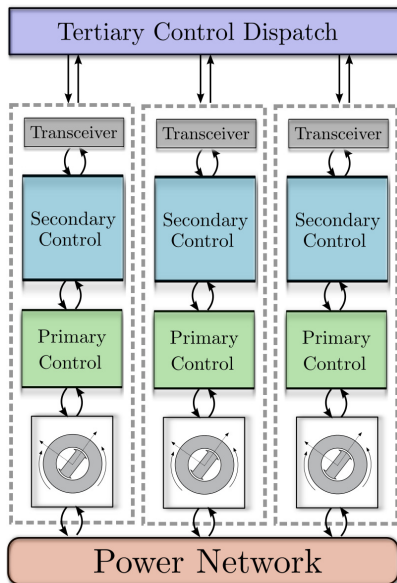


- **Electricity** is the foundation of technological civilization
- **Hierarchical** grid: generate/transmit/consume
- **Challenges:** multi-scale, nonlinear, & complex

What are the control strategies?

Bulk Power System Control Architecture & Objectives

Hierarchy by physics and spatial/temporal/centralization scales



3. **Tertiary control** (offline)

- Goal: optimize operation
- Strategy: centralized & forecast

2. **Secondary control** (minutes)

- Goal: maintain operating point
- Strategy: centralized

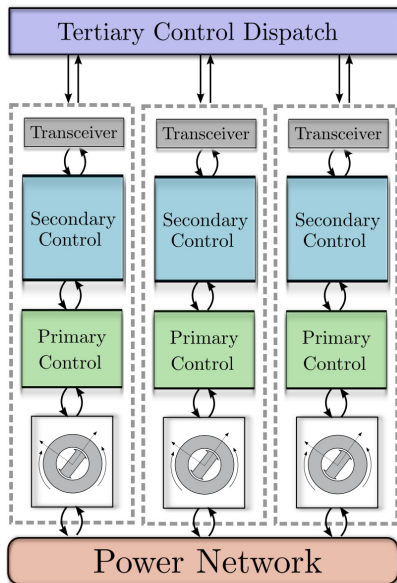
1. **Primary control** (real-time)

- Goal: stabilization & load sharing
- Strategy: decentralized

Q: Is this layered & hierarchical architecture still appropriate for tomorrow's power system?

Bulk Power System Control Architecture & Objectives

Hierarchy by physics and spatial/temporal/centralization scales



3. Tertiary control (offline)

- Goal: optimize operation
- Strategy: centralized & forecast

2. Secondary control (minutes)

- Goal: maintain operating point
- Strategy: centralized

1. Primary control (real-time)

- Goal: stabilization & load sharing
- Strategy: decentralized

Q: Is this layered & hierarchical architecture still appropriate for tomorrow's power system?

Two Major Trends



(New York Magazine)

Trend 1: Physical Volatility

- 1 bulk distributed generation, (de)regulation
- 2 growing demand & old infrastructure



lowered inertia &
robustness margins

Trend 2: Technological Advances

- 1 flexible loads, sensors & actuators
(spinning reserves, PMUs, FACTS)
- 2 control of cyber-physical systems

⇒ cyber-coordination layer for smart grid

Two Major Trends



(New York Magazine)

Trend 1: Physical Volatility

- 1 bulk distributed generation, (de)regulation
- 2 growing demand & old infrastructure



lowered inertia &
robustness margins

Trend 2: Technological Advances

- 1 flexible loads, sensors & actuators
(spinning reserves, PMUs, FACTS)
- 2 control of cyber-physical systems

⇒ cyber-coordination layer for smart grid



(Electronic Component News)

Outline

Introduction & Project Samples

Distributed Control in Microgrids

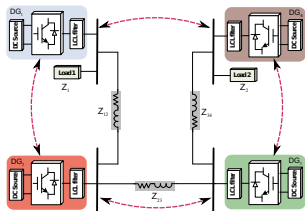
- Primary Control

- Tertiary control

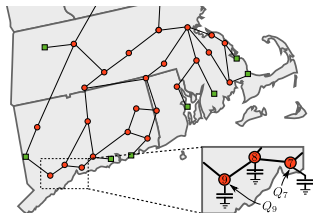
- Secondary Control

Smart Grid Project Samples

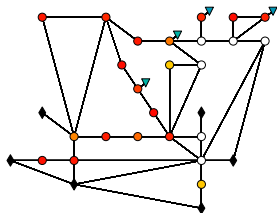
Cooperative Inverter Control



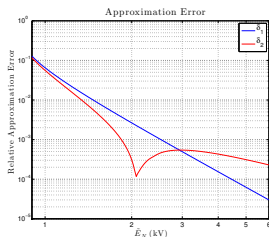
Voltage Stability/Collapse



Optimal/Sparse Voltage Support



Power Flow Approximations



Relevant Publications



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Voltage Collapse in Complex Power Grids](#). February 2015. Note: Submitted.



J. W. Simpson-Porco, Q. Shafiee, F. Dörfler, J. C. Vasquez, J. M. Guerrero, and F. Bullo. [Secondary Frequency and Voltage Control in Islanded Microgrids via Distributed Averaging](#). *IEEE Transactions on Industrial Electronics*, Sept. 2014. Note: Submitted.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [On Resistive Networks of Constant Power Devices](#). *IEEE Transactions on Circuits & Systems II: Express Briefs*, Nov. 2014. Note: To Appear.



F. Dörfler, J. W. Simpson-Porco, and F. Bullo. [Breaking the Hierarchy: Distributed Control & Economic Optimality in Microgrids](#). *IEEE Transactions on Control of Network Systems*, January 2014. Note: Submitted.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Voltage stabilization in microgrids via quadratic droop control](#). *IEEE Conference on Decision and Control*, Florence, Italy, pages 7582-7589, December 2013.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Synchronization and Power-Sharing for Droop-Controlled Inverters in Islanded Microgrids](#). *Automatica*, 49(9):2603-2611, 2013.



J. W. Simpson-Porco and F. Bullo. [Contraction Theory on Riemannian Manifolds](#) *Systems & Control Letters*, 65:74-80, 2014.



D. C. McKay *et al.* . [Low-temperature, high-density magneto-optical trapping of potassium using the open 4S-5P transition at 405 nm](#). *Phys. Rev. A*, 84:063420, 2011.

Research supported by



NSERC
CRSNG

Relevant Publications



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Voltage Collapse in Complex Power Grids](#). February 2015. Note: Submitted.



J. W. Simpson-Porco, Q. Shafiee, F. Dörfler, J. C. Vasquez, J. M. Guerrero, and F. Bullo. [Secondary Frequency and Voltage Control in Islanded Microgrids via Distributed Averaging](#). *IEEE Transactions on Industrial Electronics*, Sept. 2014. Note: Submitted.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [On Resistive Networks of Constant Power Devices](#). *IEEE Transactions on Circuits & Systems II: Express Briefs*, Nov. 2014. Note: To Appear.



F. Dörfler, J. W. Simpson-Porco, and F. Bullo. [Breaking the Hierarchy: Distributed Control & Economic Optimality in Microgrids](#). *IEEE Transactions on Control of Network Systems*, January 2014. Note: Submitted.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Voltage stabilization in microgrids via quadratic droop control](#). *IEEE Conference on Decision and Control*, Florence, Italy, pages 7582-7589, December 2013.



J. W. Simpson-Porco, F. Dörfler, and F. Bullo. [Synchronization and Power-Sharing for Droop-Controlled Inverters in Islanded Microgrids](#). *Automatica*, 49(9):2603-2611, 2013.



J. W. Simpson-Porco and F. Bullo. [Contraction Theory on Riemannian Manifolds](#) *Systems & Control Letters*, 65:74-80, 2014.



D. C. McKay *et al.* . [Low-temperature, high-density magneto-optical trapping of potassium using the open 4S-5P transition at 405 nm](#). *Phys. Rev. A*, 84:063420, 2011.

Research supported by



**NSERC
CRSNG**

Microgrids

Structure

- low-voltage distribution networks
- small-footprint & *islanded*
- autonomously managed

Applications

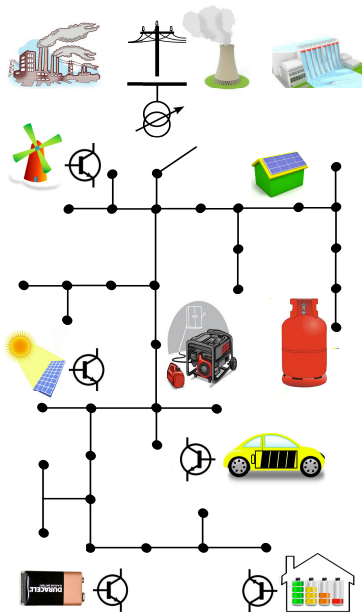
- hospitals, military, campuses, large vehicles, & isolated communities

Benefits

- naturally distributed for renewables
- scalable, efficient, & reliable

Operational challenges

- fast dynamics & low inertia
- plug'n'play & no central authority



Microgrids

Structure

- low-voltage distribution networks
- small-footprint & *islanded*
- autonomously managed

Applications

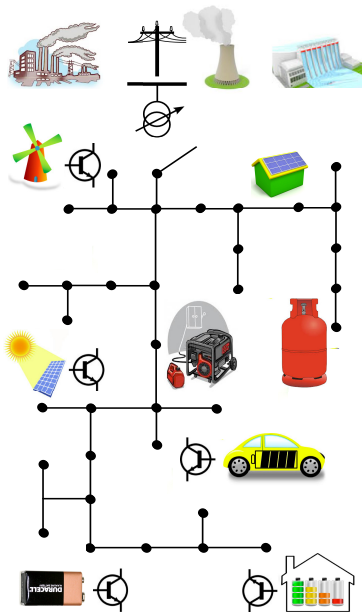
- hospitals, military, campuses, large vehicles, & isolated communities

Benefits

- naturally distributed for renewables
- scalable, efficient, & reliable

Operational challenges

- fast dynamics & low inertia
- plug'n'play & no central authority



Modeling I: AC circuits

① **Loads (●) and Inverters (■)**

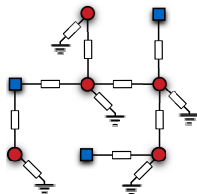
② **Quasi-Synchronous:** $\omega \simeq \omega^* \Rightarrow V_i = E_i e^{j\theta_i}$

③ **Load Model:** ZIP Loads (today, constant power)

④ **Coupling Laws:** Kirchoff and Ohm

⑤ **Identical Line Materials:** $R_{ij}/X_{ij} = \text{const.}$ (today, lossless $R_{ij}/X_{ij} = 0$)

⑥ **Decoupling:** $P_i \approx P_i(\theta)$ & $Q_i \approx Q_i(E)$ (normal operating conditions)



Modeling I: AC circuits

① **Loads (●) and Inverters (■)**

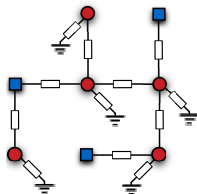
② **Quasi-Synchronous:** $\omega \simeq \omega^* \Rightarrow V_i = E_i e^{j\theta_i}$

③ **Load Model:** ZIP Loads (today, constant power)

④ **Coupling Laws:** Kirchoff and Ohm

⑤ **Identical Line Materials:** $R_{ij}/X_{ij} = \text{const.}$ (today, lossless $R_{ij}/X_{ij} = 0$)

⑥ **Decoupling:** $P_i \approx P_i(\theta)$ & $Q_i \approx Q_i(E)$ (normal operating conditions)



- active power: $P_i = \sum_j B_{ij} E_i E_j \sin(\theta_i - \theta_j) + G_{ij} E_i E_j \cos(\theta_i - \theta_j)$
- reactive power: $Q_i = -\sum_j B_{ij} E_i E_j \cos(\theta_i - \theta_j) + G_{ij} E_i E_j \sin(\theta_i - \theta_j)$

Modeling I: AC circuits

① **Loads (●) and Inverters (■)**

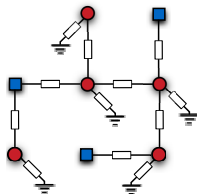
② **Quasi-Synchronous:** $\omega \simeq \omega^* \Rightarrow V_i = E_i e^{j\theta_i}$

③ **Load Model:** ZIP Loads (today, constant power)

④ **Coupling Laws:** Kirchoff and Ohm

⑤ **Identical Line Materials:** $R_{ij}/X_{ij} = \text{const.}$ (today, lossless $R_{ij}/X_{ij} = 0$)

⑥ **Decoupling:** $P_i \approx P_i(\theta)$ & $Q_i \approx Q_i(E)$ (normal operating conditions)



Modeling I: AC circuits

① **Loads (●) and Inverters (■)**

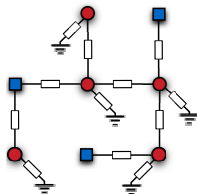
② **Quasi-Synchronous:** $\omega \simeq \omega^* \Rightarrow V_i = E_i e^{j\theta_i}$

③ **Load Model:** ZIP Loads (today, constant power)

④ **Coupling Laws:** Kirchoff and Ohm

⑤ **Identical Line Materials:** $R_{ij}/X_{ij} = \text{const.}$ (today, lossless $R_{ij}/X_{ij} = 0$)

⑥ **Decoupling:** $P_i \approx P_i(\theta)$ & $Q_i \approx Q_i(E)$ (normal operating conditions)



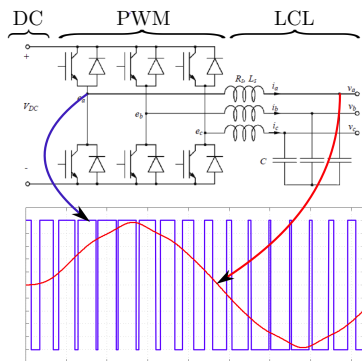
- trigonometric active power flow: $P_i(\theta) = \sum_j B_{ij} \sin(\theta_i - \theta_j)$
- quadratic reactive power flow: $Q_i(E) = -\sum_j B_{ij} E_i E_j$

Modeling II: Inverter-interfaced distributed gen.

also applies to frequency-responsive loads

Power **inverters** are ...

- **interface** between AC grid and DC or variable AC sources
- operated as **controllable** ideal voltage sources



Assumptions:

- Fast, stable inner-loops
(voltage/current/impedance)
- Balanced 3-phase operation

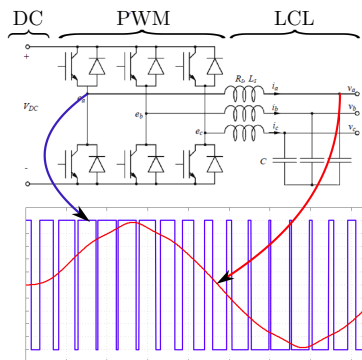
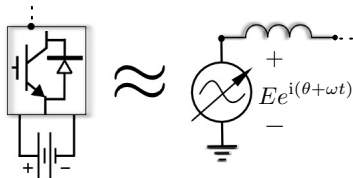
Modeling II: Inverter-interfaced distributed gen.

also applies to frequency-responsive loads

Power **inverters** are ...

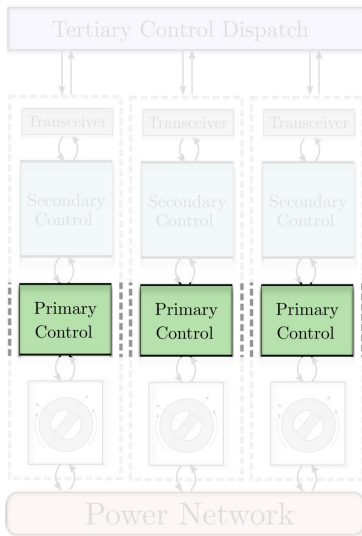
- **interface** between AC grid and DC or variable AC sources
- operated as **controllable** ideal voltage sources

$$\omega_i = u_i^{\text{freq}}, \quad \tau_i \dot{E}_i = u_i^{\text{volt}}$$



Assumptions:

- Fast, stable inner-loops
(voltage/current/impedance)
- Balanced 3-phase operation



Open-Loop System & Control Objectives

Frequency Open-Loop

Inverter Dynamics:

$$\omega_i = \dot{\theta}_i = u_i^{\text{freq}}$$

$$P_i(\theta) = \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

Load Active Power Balance:

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

Voltage Open-Loop

Inverter Dynamics:

$$\tau_i \dot{E}_i = u_i^{\text{volt}}$$

$$Q_i(E) = \sum_j B_{ij} E_i E_j$$

Load Reactive Power Balance:

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$

Primary Control Objectives:

- 1 **Stabilization:** Balance system for variable loads
- 2 **Load Sharing:** Power injection proportional to unit capacity

Decentralized Primary Control (aka Droop Control)

A grid-forming control strategy

Key Idea: emulate self-organizing generator dynamics

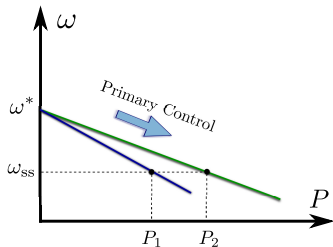
Decentralized Primary Control (aka Droop Control)

A grid-forming control strategy

Key Idea: emulate self-organizing generator dynamics

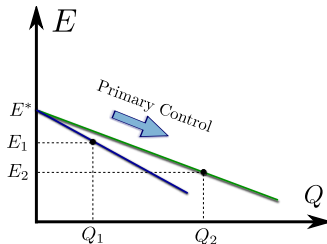
Frequency Droop Control

$$\omega_i = \omega^* - m_i P_i(\theta)$$



Voltage Droop Control

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E)$$



Spring Network Interpretations of Equilibria

Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

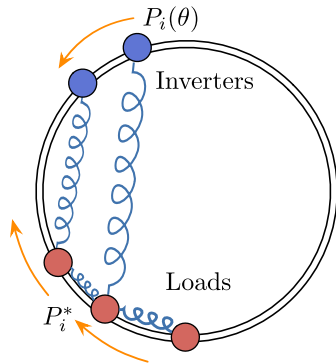
Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$

Spring Network Interpretations of Equilibria

Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$



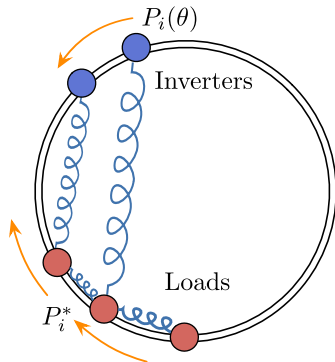
Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$

Spring Network Interpretations of Equilibria

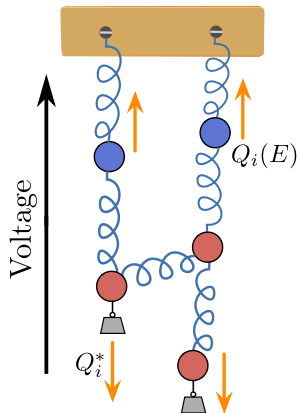
Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$



Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$



Droop Control Stability Conditions

Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

$$\dot{\theta}_i = -m_i \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

Theorem: Frequency Stability

(J. Simpson-Porco, F.D., & F.B., '12)

$\exists!$ loc. exp. stable angle equilibrium θ_{eq} iff

$$\frac{(\text{edge power flow})_{ij}}{B_{ij}} < 1$$

for all branches of microgrid.

nec. and suff.

Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$

$$\tau_i \dot{E}_i = -(E_i - E_i^*) - n_i \sum_j B_{ij} E_i E_j$$

Theorem: Voltage Stability

(J. Simpson-Porco, F.D., & F.B., '14)

$\exists!$ loc. exp. stable voltage equilibrium point E_{eq} if

$$\frac{4 \cdot \text{load} \cdot (\text{impedance})}{(\text{nominal voltage})^2} < 1$$

for all load buses of microgrid.

suff. and tight

Droop Control Stability Conditions

Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

$$\dot{\theta}_i = -m_i \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

Theorem: Frequency Stability

(J. Simpson-Porco, F.D., & F.B., '12)

∃! loc. exp. stable angle equilibrium θ_{eq} iff

$$\frac{(\text{edge power flow})_{ij}}{B_{ij}} < 1$$

for all branches of microgrid.

nec. and suff.

Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$

$$\tau_i \dot{E}_i = -(E_i - E_i^*) - n_i \sum_j B_{ij} E_i E_j$$

Theorem: Voltage Stability

(J. Simpson-Porco, F.D., & F.B., '14)

∃! loc. exp. stable voltage equilibrium point E_{eq} if

$$\frac{4 \cdot \text{load} \cdot (\text{impedance})}{(\text{nominal voltage})^2} < 1$$

for all load buses of microgrid.

suff. and tight

Droop Control Stability Conditions

Frequency Droop Control

$$0 = P_i^* - \sum_j B_{ij} \sin(\theta_i - \theta_j)$$
$$\dot{\theta}_i = -m_i \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

Theorem: Frequency Stability

(J. Simpson-Porco, F.D., & F.B., '12)

$\exists!$ loc. exp. stable angle equilibrium θ_{eq} iff

$$\frac{(\text{edge power flow})_{ij}}{B_{ij}} < 1$$

for all branches of microgrid.

nec. and suff.

Voltage Droop Control

$$0 = Q_i^* - \sum_j B_{ij} E_i E_j$$
$$\tau_i \dot{E}_i = -(E_i - E_i^*) - n_i \sum_j B_{ij} E_i E_j$$

Theorem: Voltage Stability

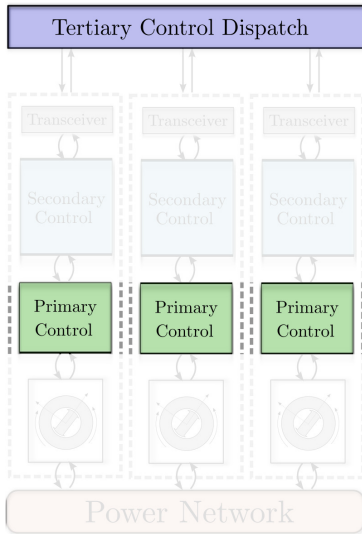
(J. Simpson-Porco, F.D., & F.B., '14)

$\exists!$ loc. exp. stable voltage equilibrium point E_{eq} if

$$\frac{4 \cdot \text{load} \cdot (\text{impedance})}{(\text{nominal voltage})^2} < 1$$

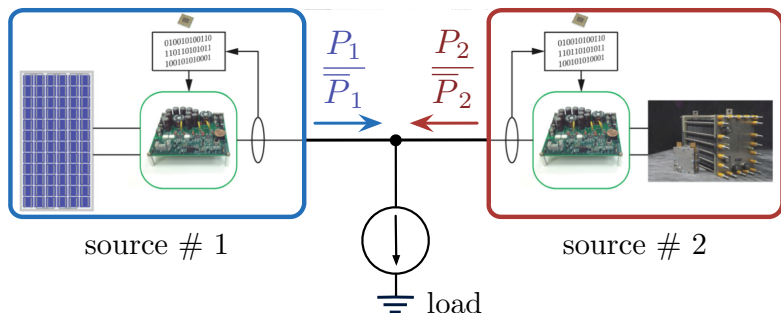
for all load buses of microgrid.

suff. and tight



Objective I: decentralized proportional load sharing

- 1) Inverters have **injection constraints**: $0 \leq P_i(\theta) \leq \bar{P}_i$
- 2) Load must be **serviceable**: $0 \leq \left| \sum_{\text{loads}} P_j^* \right| \leq \sum_{\text{inverters}} \bar{P}_j$
- 3) **Fairness**: load should be shared proportionally: $P_i(\theta) / \bar{P}_i = P_j(\theta) / \bar{P}_j$



Objective I: decentralized proportional load sharing

- 1) Inverters have **injection constraints**: $0 \leq P_i(\theta) \leq \bar{P}_i$
- 2) Load must be **serviceable**: $0 \leq \left| \sum_{\text{loads}} P_j^* \right| \leq \sum_{\text{inverters}} \bar{P}_j$
- 3) **Fairness**: load should be shared proportionally: $P_i(\theta) / \bar{P}_i = P_j(\theta) / \bar{P}_j$

Theorem (Load Sharing)

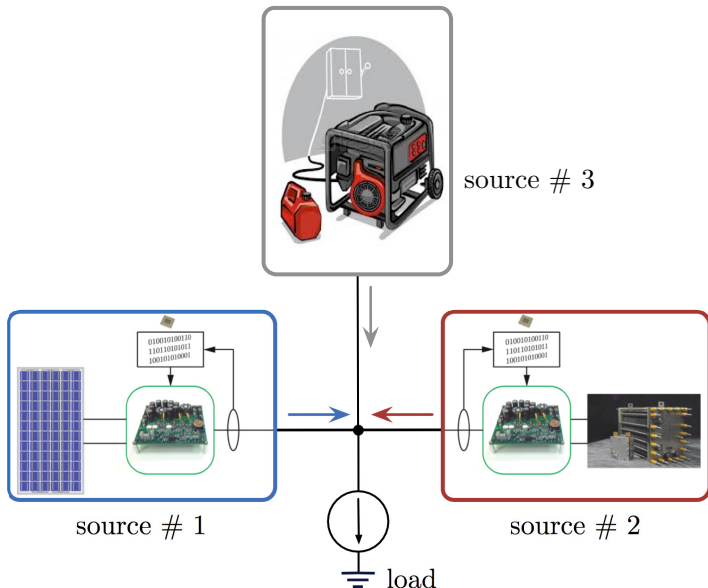
[J. Simpson-Porco, FD, & F. Bullo, '12]

If we select the controller gains such that $m_i \bar{P}_i = m_j \bar{P}_j$, then

- (i) Proportional load sharing: $P_i(\theta) / \bar{P}_i = P_j(\theta) / \bar{P}_j$
- (ii) Constraints met: $0 \leq P_i(\theta) \leq \bar{P}_i$

What if we don't like "sharing"?

proportional load sharing is not always the right objective



Objective II: optimal economic dispatch

minimize the total accumulated generation

$$\begin{array}{ll}\text{minimize } \theta \in \mathbb{T}^n, u \in \mathbb{R}^{n_I} & f(\theta) = \frac{1}{2} \sum_{\text{inverters}} \alpha_i [P_i(\theta)]^2 \\ \text{subject to} & \\ \text{load power balance:} & 0 = P_i^* - P_i(\theta) \\ \text{branch flow constraints:} & |\theta_i - \theta_j| \leq \gamma_{ij} < \pi/2 \\ \text{inverter injection constraints:} & P_i(\theta) \in [0, \bar{P}_i]\end{array}$$

Objective II: optimal economic dispatch

minimize the total accumulated generation

$$\begin{aligned} & \text{minimize } \theta \in \mathbb{T}^n, u \in \mathbb{R}^{n_I} & f(\theta) &= \frac{1}{2} \sum_{\text{inverters}} \alpha_i [P_i(\theta)]^2 \\ & \text{subject to} & & \\ & \quad \text{load power balance:} & 0 &= P_i^* - P_i(\theta) \\ & \quad \text{branch flow constraints:} & |\theta_i - \theta_j| &\leq \gamma_{ij} < \pi/2 \\ & \quad \text{inverter injection constraints:} & P_i(\theta) &\in [0, \bar{P}_i] \end{aligned}$$

Conventional: Offline, Centralized, Model & Load Forecast

Objective II: optimal economic dispatch

minimize the total accumulated generation

$$\begin{aligned} &\text{minimize } \theta \in \mathbb{T}^n, u \in \mathbb{R}^{n_I} & f(\theta) &= \frac{1}{2} \sum_{\text{inverters}} \alpha_i [P_i(\theta)]^2 \\ &\text{subject to} & & \\ &\quad \text{load power balance:} & 0 &= P_i^* - P_i(\theta) \\ &\quad \text{branch flow constraints:} & |\theta_i - \theta_j| &\leq \gamma_{ij} < \pi/2 \\ &\quad \text{inverter injection constraints:} & P_i(\theta) &\in [0, \bar{P}_i] \end{aligned}$$

Conventional: Offline, Centralized, Model & Load Forecast

Autonomous Microgrid: On-line, decentralized, no model, no forecasts

Objective II: decentralized economic dispatch optimization

Insight: droop-controlled microgrid = decentralized primal algorithm

Dispatch through droop control [H. Bouattour, FD, J. Simpson-Porco, & F. Bullo, '13]

The following statements are equivalent:

- (i) econ. dispatch with cost coeffs. α_i is **strictly** feasible w/ global minimizer θ^* ;
- (ii) $\exists$ droop coefficients m_i s.t. the microgrid possesses a unique & loc. exp. stable operating point θ^* satisfying $P_i(\theta^*) \in [0, \bar{P}_i)$.

If (i) & (ii) are true, then $P_i(\theta^*) = (\omega^* - \omega_{ss})/m_i$, & $\boxed{\frac{\alpha_i}{m_i} = \frac{\alpha_j}{m_j}}$.

• similar results for **constrained** case — though not fully decentralized

Objective II: decentralized economic dispatch optimization

Insight: droop-controlled microgrid = decentralized primal algorithm

Dispatch through droop control [H. Bouattour, FD, J. Simpson-Porco, & F. Bullo, '13]

The following statements are equivalent:

- (i) econ. dispatch with cost coeffs. α_i is **strictly** feasible w/ global minimizer θ^* ;
- (ii) $\exists$ droop coefficients m_i s.t. the microgrid possesses a unique & loc. exp. stable operating point θ^* satisfying $P_i(\theta^*) \in [0, \bar{P}_i)$.

If (i) & (ii) are true, then $P_i(\theta^*) = (\omega^* - \omega_{ss})/m_i$, & $\boxed{\frac{\alpha_i}{m_i} = \frac{\alpha_j}{m_j}}$.

• similar results for **constrained** case — though not fully decentralized

Objective II: decentralized economic dispatch optimization

Insight: droop-controlled microgrid = decentralized primal algorithm

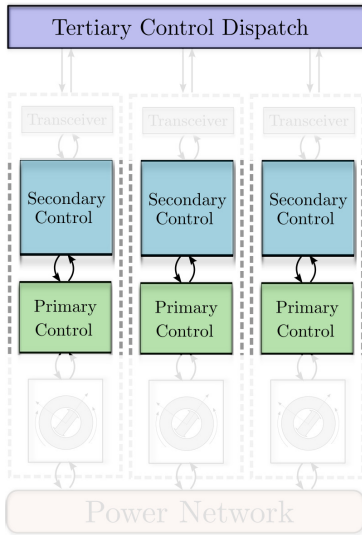
Dispatch through droop control [H. Bouattour, FD, J. Simpson-Porco, & F. Bullo, '13]

The following statements are equivalent:

- (i) econ. dispatch with cost coeffs. α_i is **strictly** feasible w/ global minimizer θ^* ;
- (ii) $\exists$ droop coefficients m_i s.t. the microgrid possesses a unique & loc. exp. stable operating point θ^* satisfying $P_i(\theta^*) \in [0, \bar{P}_i)$.

If (i) & (ii) are true, then $P_i(\theta^*) = (\omega^* - \omega_{ss})/m_i$, & $\boxed{\frac{\alpha_i}{m_i} = \frac{\alpha_j}{m_j}}$.

- similar results for **constrained** case — though not fully decentralized



Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

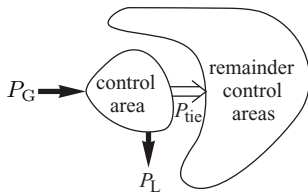
Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

Interconnected Systems

- **Centralized** automatic generation control (AGC)



Isolated Systems

- **Decentralized** PI control

Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

Interconnected Systems

- **Centralized** automatic generation control (AGC)

P_G

P_L

centralized &
not applicable
in microgrids

Isolated Systems

- **Decentralized** PI control

Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

Interconnected Systems

- **Centralized** automatic generation control (AGC)

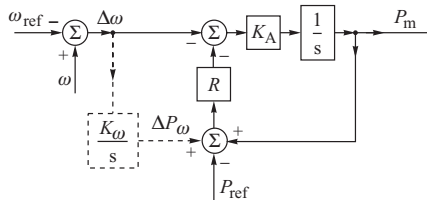
centralized &
not applicable
in microgrids

P_G

P_L

Isolated Systems

- **Decentralized** PI control



Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

Interconnected Systems

- Centralized automatic generation control (AGC)

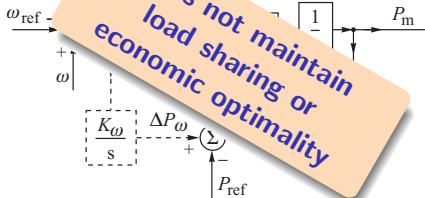
P_G

centralized &
not applicable
in microgrids

P_L

Isolated Systems

- Decentralized PI control



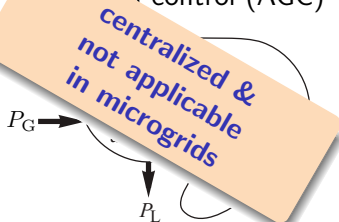
Secondary frequency control in power networks

Problem: steady-state frequency deviation ($\omega_{ss} \neq \omega^*$)

Solution: integral control on frequency error

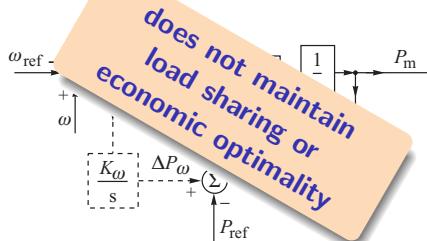
Interconnected Systems

- Centralized automatic generation control (AGC)



Isolated Systems

- Decentralized PI control



Microgrids require **distributed (!)** secondary control strategies.

Distributed Averaging PI (DAPI) Frequency Control

$$\omega_i = \omega^* - m_i P_i(\theta) - \Omega_i$$

$$k_i \dot{\Omega}_i = (\omega_i - \omega^*) - \sum_{j \in \text{inverters}} a_{ij} \cdot (\Omega_i - \Omega_j)$$

- 1 no tuning, no model dependence
- 2 weak comm. requirements
- 3 preserves optimal dispatch

Simple & Plug'n'play

Theorem: Stability of DAPI

[J. Simpson-Porco, FD, & F. Bullo, '12]

DAPI Stable



Primary Droop Stable

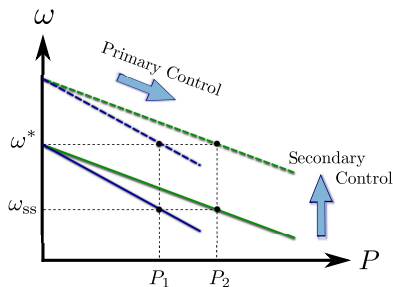
Distributed Averaging PI (DAPI) Frequency Control

$$\omega_i = \omega^* - m_i P_i(\theta) - \Omega_i$$

$$k_i \dot{\Omega}_i = (\omega_i - \omega^*) - \sum_{j \subseteq \text{inverters}} a_{ij} \cdot (\Omega_i - \Omega_j)$$

- 1 no tuning, no model dependence
- 2 weak comm. requirements
- 3 preserves optimal dispatch

Simple & Plug'n'play



Theorem: Stability of DAPI

[J. Simpson-Porco, FD, & F. Bullo, '12]

DAPI Stable



Primary Droop Stable

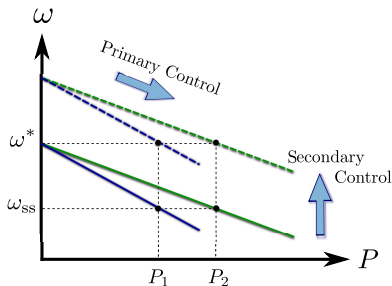
Distributed Averaging PI (DAPI) Frequency Control

$$\omega_i = \omega^* - m_i P_i(\theta) - \Omega_i$$

$$k_i \dot{\Omega}_i = (\omega_i - \omega^*) - \sum_{j \subseteq \text{inverters}} a_{ij} \cdot (\Omega_i - \Omega_j)$$

- 1 no tuning, no model dependence
- 2 weak comm. requirements
- 3 preserves optimal dispatch

Simple & Plug'n'play



Theorem: Stability of DAPI

[J. Simpson-Porco, FD, & F. Bullo, '12]

DAPI Stable



Primary Droop Stable

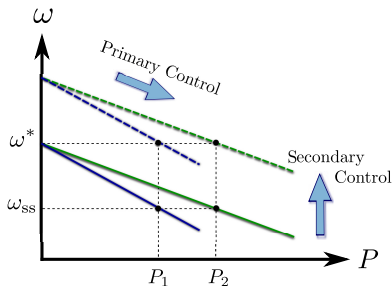
Distributed Averaging PI (DAPI) Frequency Control

$$\omega_i = \omega^* - m_i P_i(\theta) - \Omega_i$$

$$k_i \dot{\Omega}_i = (\omega_i - \omega^*) - \sum_{j \subseteq \text{inverters}} a_{ij} \cdot (\Omega_i - \Omega_j)$$

- 1 no tuning, no model dependence
- 2 weak comm. requirements
- 3 preserves optimal dispatch

Simple & Plug'n'play



Theorem: Stability of DAPI

[J. Simpson-Porco, FD, & F. Bullo, '12]

DAPI Stable



Primary Droop Stable

Distributed Averaging PI (DAPI) Voltage Control

Goals: Voltage regulation $E_i \rightarrow E^*$, load sharing $Q_i/Q_i^* = Q_j/Q_j^*$

Bad News: Unlike P/ω , these goals are *fundamentally* conflicting.

Key Idea: Trade-off between voltage regulation / Q-Sharing

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E) - e_i$$

$$\kappa_i \dot{e}_i = \beta_i (E_i - E_i^*) - \sum_{j \in \text{Inverters}} b_{ij} \cdot \left(\frac{Q_i}{Q_i^*} - \frac{Q_j}{Q_j^*} \right)$$

Tuning Intuition:

- 1 $\beta_i \gg \sum_j b_{ij} \implies$ voltage regulation
- 2 $\beta_i \ll \sum_j b_{ij} \implies$ Q-Sharing

Distributed Averaging PI (DAPI) Voltage Control

Goals: Voltage regulation $E_i \rightarrow E^*$, load sharing $Q_i/Q_i^* = Q_j/Q_j^*$

Bad News: Unlike P/ω , these goals are *fundamentally* conflicting.

Key Idea: Trade-off between voltage regulation / Q-Sharing

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E) - e_i$$

$$\kappa_i \dot{e}_i = \beta_i (E_i - E_i^*) - \sum_{j \in \text{Inverters}} b_{ij} \cdot \left(\frac{Q_i}{Q_i^*} - \frac{Q_j}{Q_j^*} \right)$$

Tuning Intuition:

- 1 $\beta_i \gg \sum_j b_{ij} \implies$ voltage regulation
- 2 $\beta_i \ll \sum_j b_{ij} \implies$ Q-Sharing

Distributed Averaging PI (DAPI) Voltage Control

Goals: Voltage regulation $E_i \rightarrow E^*$, load sharing $Q_i/Q_i^* = Q_j/Q_j^*$

Bad News: Unlike P/ω , these goals are *fundamentally* conflicting.

Key Idea: Trade-off between voltage regulation / Q-Sharing

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E) - e_i$$

$$\kappa_i \dot{e}_i = \beta_i (E_i - E_i^*) - \sum_{j \in \text{inverters}} b_{ij} \cdot \left(\frac{Q_i}{Q_i^*} - \frac{Q_j}{Q_j^*} \right)$$

Tuning Intuition:

- 1 $\beta_i \gg \sum_j b_{ij} \Rightarrow$ voltage regulation
- 2 $\beta_i \ll \sum_j b_{ij} \Rightarrow$ Q-Sharing

Distributed Averaging PI (DAPI) Voltage Control

Goals: Voltage regulation $E_i \rightarrow E^*$, load sharing $Q_i/Q_i^* = Q_j/Q_j^*$

Bad News: Unlike P/ω , these goals are *fundamentally* conflicting.

Key Idea: Trade-off between voltage regulation / Q-Sharing

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E) - e_i$$

$$\kappa_i \dot{e}_i = \beta_i (E_i - E_i^*) - \sum_{j \subseteq \text{inverters}} b_{ij} \cdot \left(\frac{Q_i}{Q_i^*} - \frac{Q_j}{Q_j^*} \right)$$

Tuning Intuition:

- 1 $\beta_i \gg \sum_j b_{ij} \Rightarrow$ voltage regulation
- 2 $\beta_i \ll \sum_j b_{ij} \Rightarrow$ Q-Sharing

Distributed Averaging PI (DAPI) Voltage Control

Goals: Voltage regulation $E_i \rightarrow E^*$, load sharing $Q_i/Q_i^* = Q_j/Q_j^*$

Bad News: Unlike P/ω , these goals are *fundamentally* conflicting.

Key Idea: Trade-off between voltage regulation / Q-Sharing

$$\tau_i \dot{E}_i = -(E_i - E^*) - n_i Q_i(E) - e_i$$

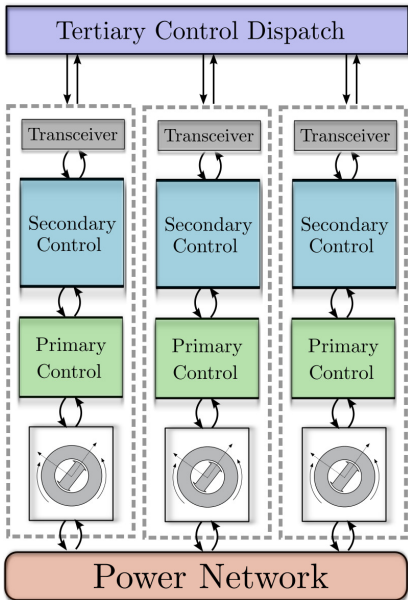
$$\kappa_i \dot{e}_i = \beta_i (E_i - E_i^*) - \sum_{j \subseteq \text{inverters}} b_{ij} \cdot \left(\frac{Q_i}{Q_i^*} - \frac{Q_j}{Q_j^*} \right)$$

Tuning Intuition:

- ① $\beta_i \gg \sum_j b_{ij} \implies$ voltage regulation
- ② $\beta_i \ll \sum_j b_{ij} \implies$ Q-Sharing

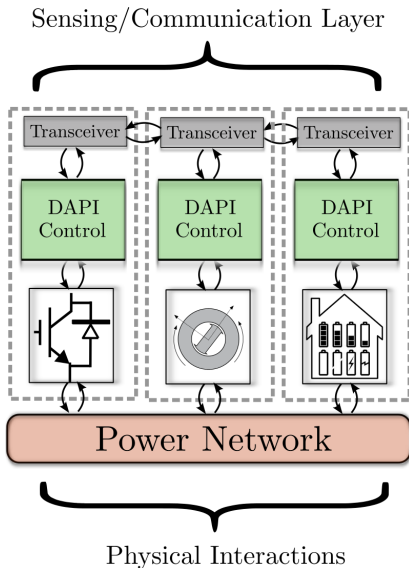
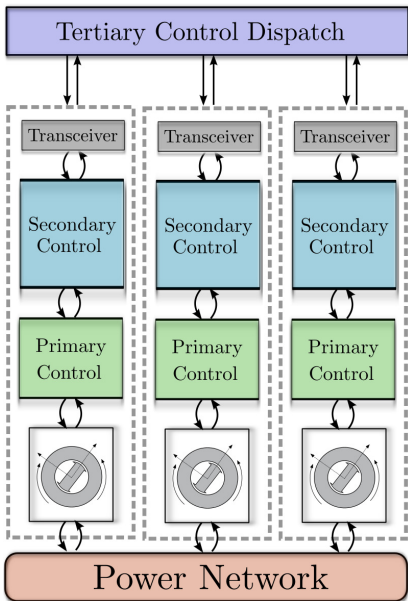
Plug'n'play architecture

flat hierarchy, distributed, no time-scale separations, & model-free



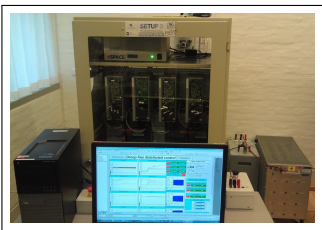
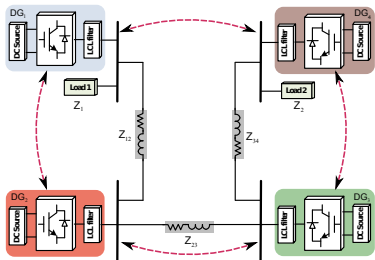
Plug'n'play architecture

flat hierarchy, distributed, no time-scale separations, & model-free



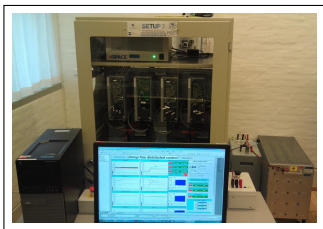
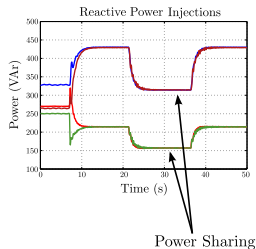
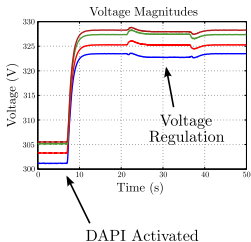
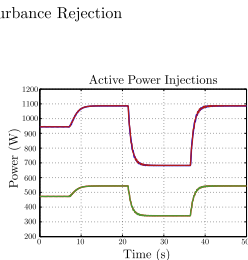
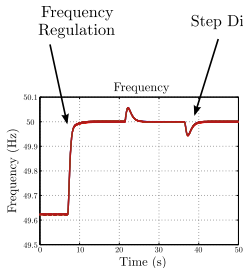
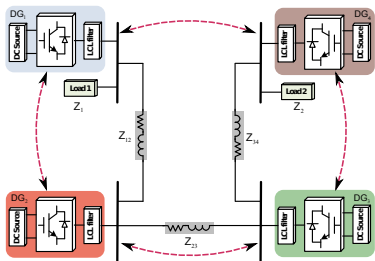
Experimental Validation of DAPI Control

Experiments @ Aalborg University with Q. Shafiee, J. C. Vasquez & J. M. Guerrero



Experimental Validation of DAPI Control

Experiments @ Aalborg University with Q. Shafiee, J. C. Vasquez & J. M. Guerrero



Ongoing Theoretical and Practical Challenges

- ① Interaction w/ **price dynamics**
- ② Cyber-security in DAPI control
- ③ **Performance limits** of decentralized control
- ④ Large-scale study w/ NS-3 comm. & more detailed load models

Summary

Distributed Inverter Control

- Primary control stability
- Distributed PI controllers
- Primary/tertiary connections
- Experiments: “It works. Really.”

More Results (not shown)

- More voltage control/opt.
- Accurate approximations

