

# Model-Free Wide-Area Monitoring of Power Grids via Cutset Voltages

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John W. Simpson-Porco & Nima Monshizadeh

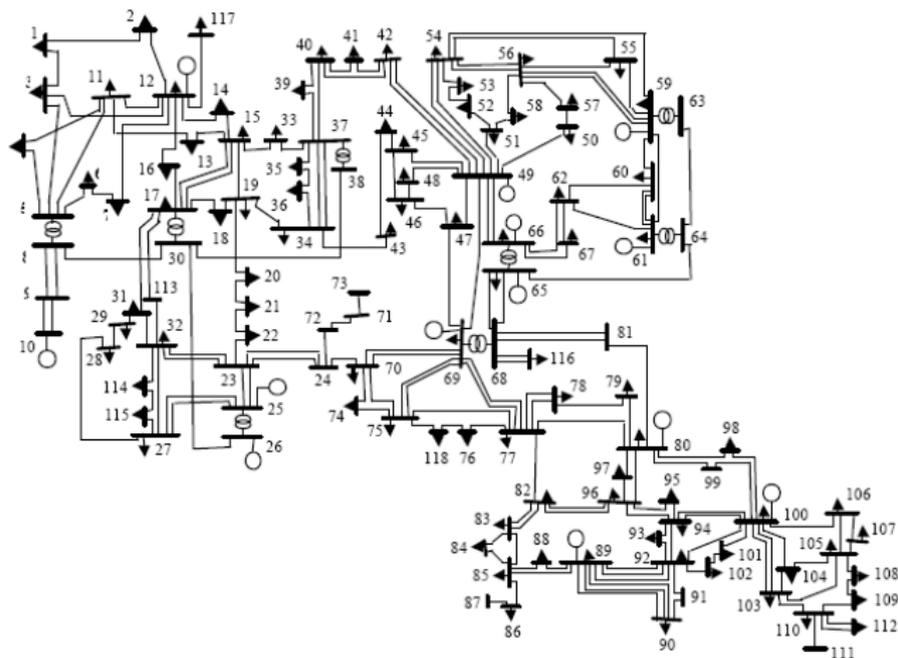


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**WATERLOO**

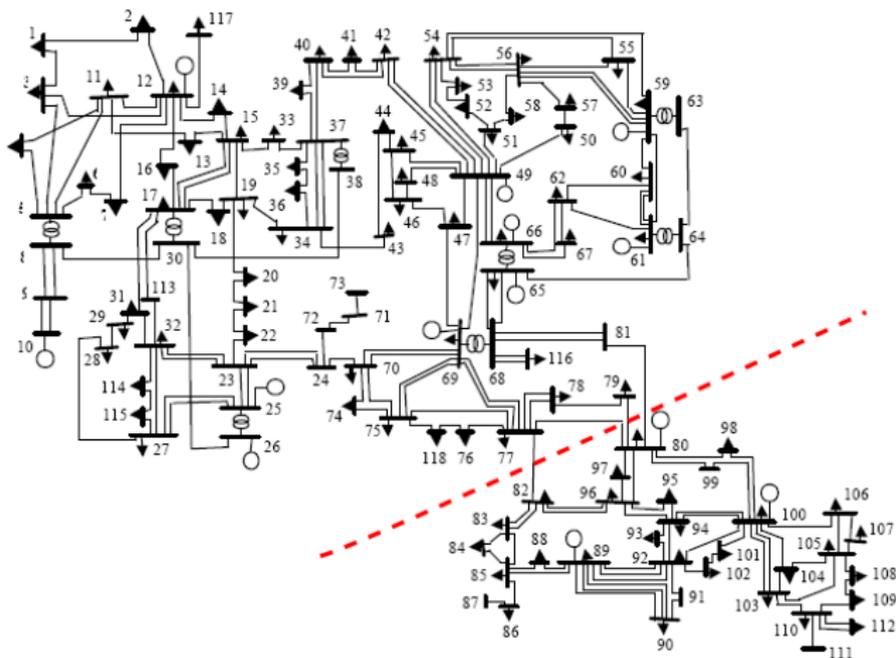


UNIVERSITY OF  
**CAMBRIDGE**

# Wide-Area Monitoring and the Power Grid



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# Basic Circuit Theory

- **Graph**  $\mathcal{G} = (\mathcal{N}, \mathcal{E})$  with **edge weights**  $g_{ij}$ ,  $g = \text{diag}(g_{ij})$
- **Incidence matrix:**  $A \in \{-1, 0, 1\}^{(\text{nodes}) \times (\text{edges})}$
- **Nodal current injections**  $I_i$  and **edge currents**  $i_{ij}$
- **Nodal voltages**  $V_i$  and **branch voltages**  $v_{ij}$

## Circuit Equations

$$I = Ai \quad (\text{KCL})$$

$$v = A^T V \quad (\text{KVL})$$

$$i = gv \quad (\text{Ohm})$$

Nodal Equations  $I = GV$  with **conductance matrix**  $G = AgA^T$

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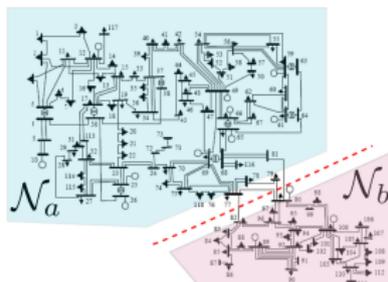
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# Basic Circuit Theory for Two-Area Circuit



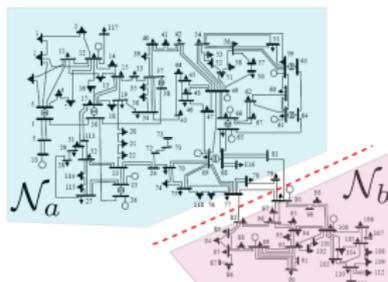
- Nodal partitioning:  $\mathcal{N} = \mathcal{N}_a \cup \mathcal{N}_b$

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# The Cutset Voltage

Dobson *et. al.*

- A **scalar, aggregated** metric for stress across a cutset

- Define the **cutset current**

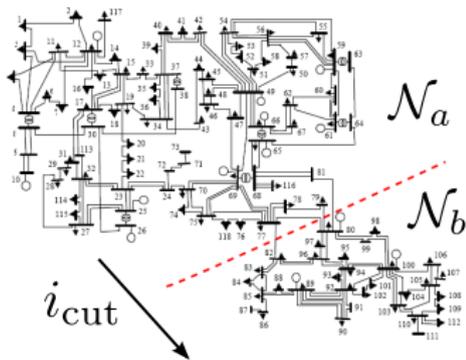
$$i_{\text{cut}} = \mathbb{1}^T i_{ab} = \sum_{e \sim (i,j) \in \mathcal{E}^{ab}} i_e.$$

- and the **cutset conductance**

$$g_{\text{cut}} = \mathbb{1}^T g_{ab} \mathbb{1} = \sum_{(i,j) \in \mathcal{E}^{ab}} g_{ij},$$

- Combining, we get the **cutset voltage**

$$v_{\text{cut}} = i_{\text{cut}} / g_{\text{cut}}$$



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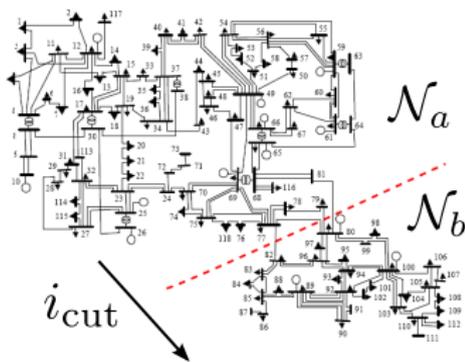
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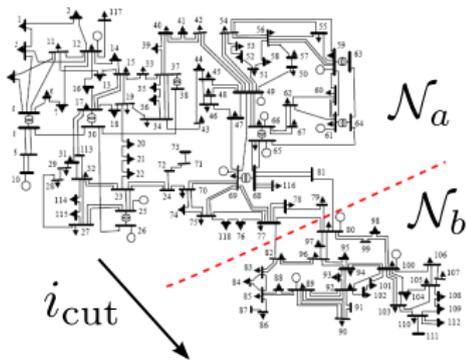
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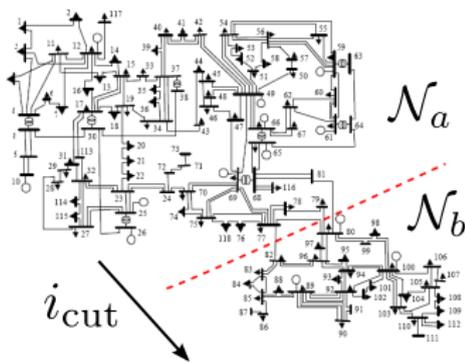
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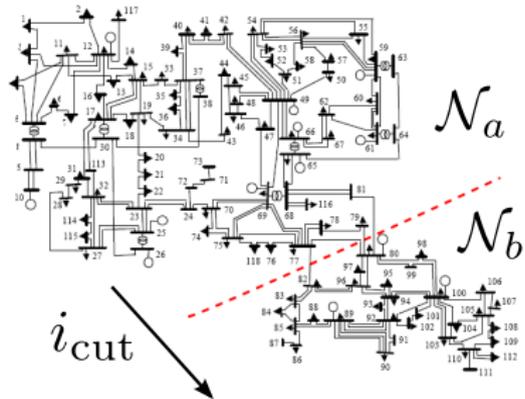
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$$v_{\text{cut}} = \frac{\sum_{(i,j) \in \mathcal{E}^{ab}} i_{ij}}{\sum_{(i,j) \in \mathcal{E}^{ab}} g_{ij}}$$



- Voltage across “average” edge in cutset
- $g_{\text{cut}}$  is **parallel** combination of conductances in cut
  - $\implies$  **Exact reduction** if voltages uniform on either side of cut!
- Decompose voltage vectors as

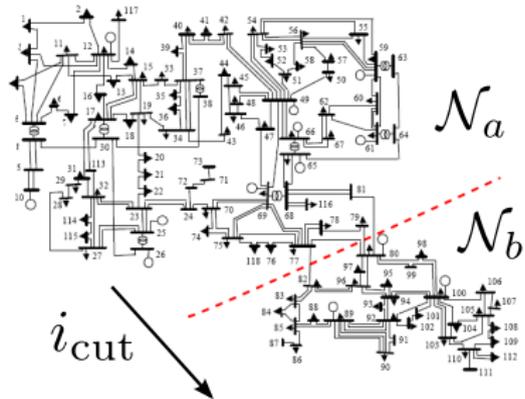
$$\begin{bmatrix} V_a \\ V_b \end{bmatrix} = \begin{bmatrix} \mu_a \mathbb{1}_a \\ \mu_b \mathbb{1}_b \end{bmatrix} + \begin{bmatrix} \tilde{V}_a \\ \tilde{V}_b \end{bmatrix}, \quad (1)$$

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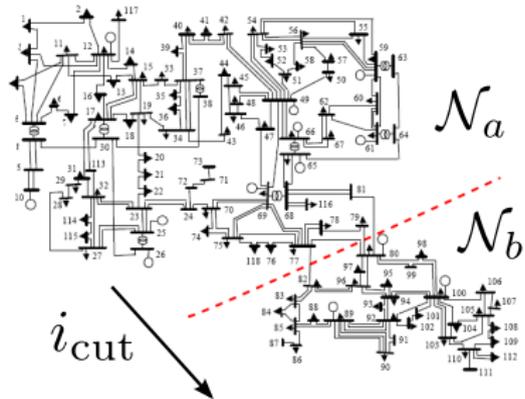
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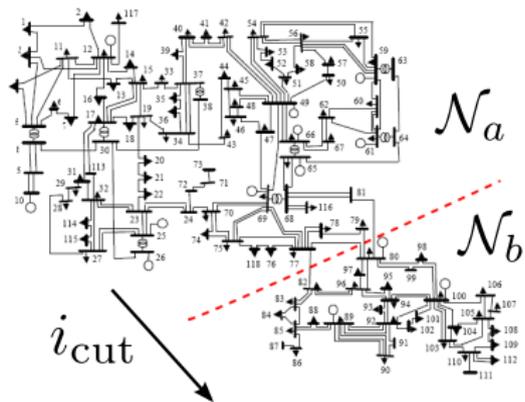
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# Result: Cutset Voltage and Average Voltage Levels

Define **weighted inter-area degree vectors**

$$g_a = -G_{ab}\mathbb{1}_b \quad g_b = -G_{ba}\mathbb{1}_a$$

and the **projection matrices**

$$\Pi_a = \mathbb{I}_a - \frac{1}{|\mathcal{N}_a|}\mathbb{1}_a\mathbb{1}_a^T, \quad \Pi_b = \mathbb{I}_b - \frac{1}{|\mathcal{N}_b|}\mathbb{1}_b\mathbb{1}_b^T,$$

## Theorem 1

The cutset voltage  $v_{\text{cut}}$  is given by

$$v_{\text{cut}} = \mu_a - \mu_b + \varepsilon_{\text{cut}}$$

where the *cutset error*  $\varepsilon_{\text{cut}}$  is

$$\varepsilon_{\text{cut}} = \frac{1}{g_{\text{cut}}} \begin{bmatrix} g_a^T \Pi_a & -g_b^T \Pi_b \end{bmatrix} \begin{bmatrix} V_a \\ V_b \end{bmatrix},$$

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The error term will vanish if:

- **Uniform Area Voltages:**  $V_a = \mu_a \mathbb{1}_a$  and  $V_b = \mu_b \mathbb{1}_b$   
 $\implies \epsilon_{\text{cut}} = 0$
- $\Pi_a g_a = 0$  and  $\Pi_b g_b = 0$  (?)

# Almost Equitable Partitions I

## Definition

Let  $\pi \triangleq \{\mathcal{N}_1, \mathcal{N}_2, \dots, \mathcal{N}_K\}$  be a partition of  $\mathcal{G} = (\mathcal{N}, \mathcal{E})$ . For any node  $i \in \mathcal{N}$  and any area  $q \in \{1, \dots, K\}$ , let

$$g_{\text{parallel}}(i, \mathcal{N}_q) \triangleq \sum_{j \in \mathcal{N}_q, \{i,j\} \in \mathcal{E}} g_{ij},$$

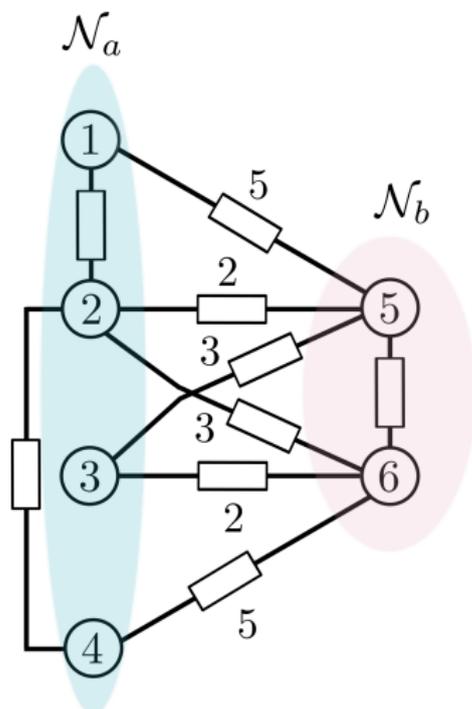
be the total parallel conductance between node  $i \in \mathcal{N}$  and area  $\mathcal{N}_q$ . We call  $\pi$  an *almost equitable partition* (AEP) of  $\mathcal{G}$  if for each pair of distinct areas  $p, q \in \{1, \dots, K\}$ , there exists a value  $g_{pq} \in \mathbb{R}$  such that

$$g_{\text{parallel}}(i, \mathcal{N}_q) = g_{pq},$$

for all nodes  $i \in \mathcal{N}_p$ .

- Every node in each area “sees” the same parallel conductance to the other areas.

## Almost Equitable Partitions II



- Conditions for AEP?

### Lemma

For two-area network  $\pi = \{\mathcal{N}_a, \mathcal{N}_b\}$ :

$\pi$  is an AEP

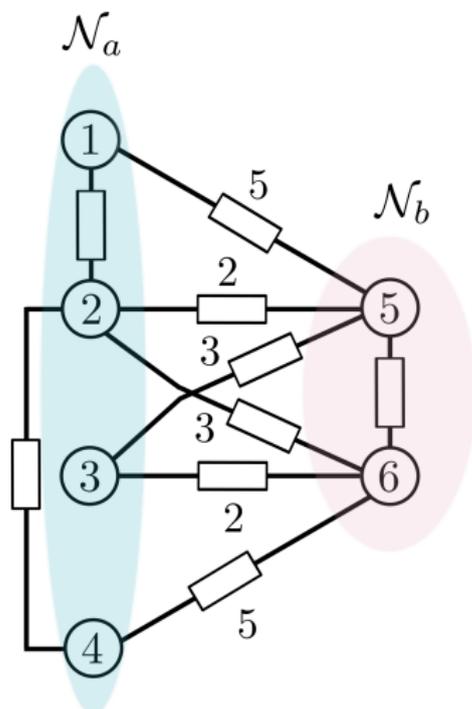
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$g_a \in \text{im}(\mathbf{1}_a)$  and  $g_b \in \text{im}(\mathbf{1}_b)$

In this example:

$$g_a = \begin{bmatrix} 5 \\ 5 \\ 5 \\ 5 \end{bmatrix} \quad g_b = \begin{bmatrix} 10 \\ 10 \end{bmatrix}$$

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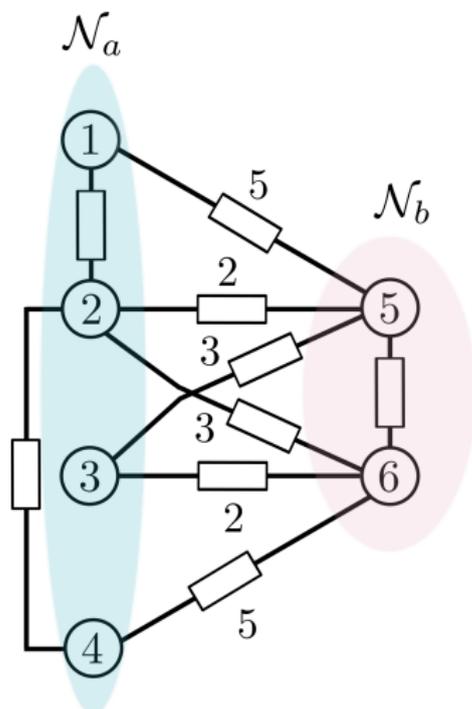
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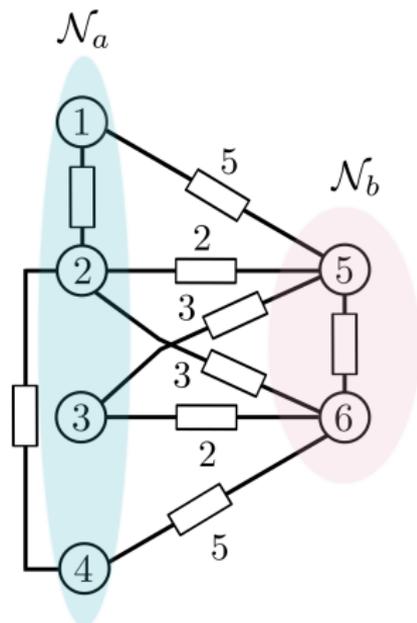
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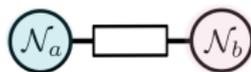
# Example



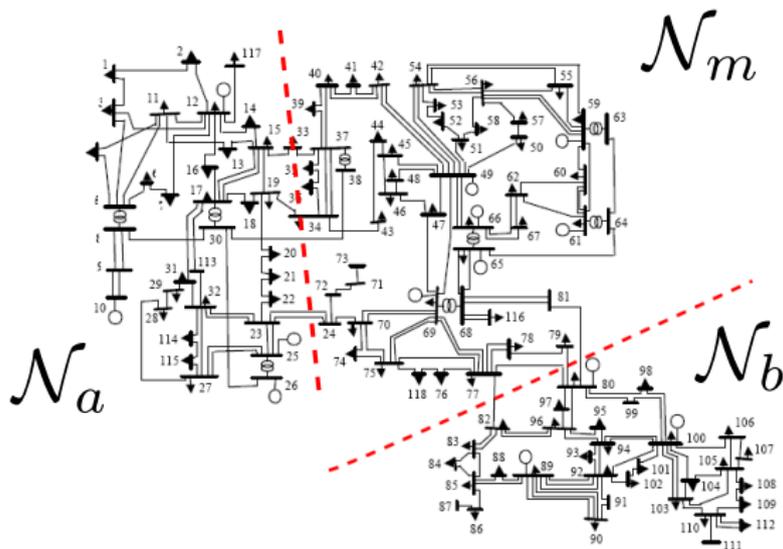
$$\mu_a = \frac{V_1 + V_2 + V_3 + V_4}{4}$$
$$\mu_b = \frac{V_5 + V_6}{2}$$



$$v_{\text{cut}} = \mu_a - \mu_b$$



# Extension to Voltage Across An Area



**Key Idea:** Kron reduction

$$\begin{bmatrix} I_a \\ I_m \\ I_b \end{bmatrix} = \begin{bmatrix} G_{aa} & G_{am} & \mathbb{0} \\ G_{ma} & G_{mm} & G_{mb} \\ \mathbb{0} & G_{bm} & G_{bb} \end{bmatrix} \begin{bmatrix} V_a \\ V_m \\ V_b \end{bmatrix} \Rightarrow \begin{bmatrix} I_a^{\text{red}} \\ I_b^{\text{red}} \end{bmatrix} = \begin{bmatrix} G_{aa}^{\text{red}} & G_{ab}^{\text{red}} \\ G_{ba}^{\text{red}} & G_{bb}^{\text{red}} \end{bmatrix} \begin{bmatrix} V_a \\ V_b \end{bmatrix}$$

# Voltage Across an Area

Dobson *et. al.*

We now have a **reduced graph**  $\mathcal{G}_{\text{red}} = (\mathcal{N}_a \cup \mathcal{N}_b, \mathcal{E}_{\text{red}})$

- Define the **current across the area**

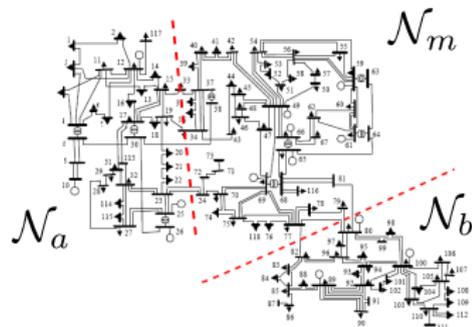
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$$g_{\text{area}} = \sum_{(i,j) \in \mathcal{E}_{\text{red}}^{ab}} g_{ij}^{\text{red}},$$

- Leading to the **area voltage**

$$v_{\text{area}} = i_{\text{cut}}^{\text{red}} / g_{\text{area}}$$



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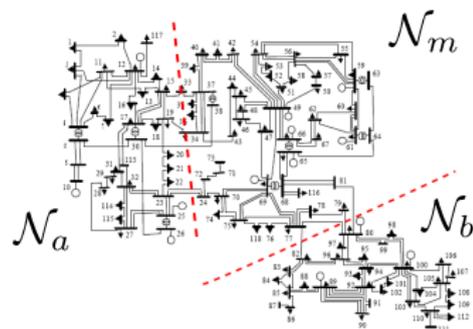
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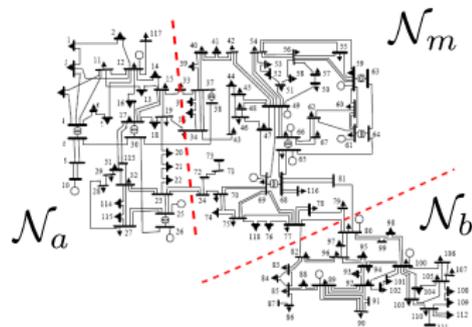
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$$v_{\text{area}} = i_{\text{cut}}^{\text{red}} / g_{\text{area}}$$



# Decomposing the Area Voltage

- Applying our cutset results, we have

## Theorem 2

The area voltage  $v_{\text{cut}}$  is given by

$$v_{\text{area}} = \mu_a - \mu_b + \varepsilon_{\text{area}}$$

where the *area error*  $\varepsilon_{\text{area}}$  is

$$\varepsilon_{\text{area}} = \frac{1}{g_{\text{area}}} \left[ (g_a^{\text{red}})^{\top} \pi_a \quad -(g_b^{\text{red}})^{\top} \pi_b \right] \begin{bmatrix} V_a \\ V_b \end{bmatrix},$$

- We know  $\varepsilon_{\text{area}} = 0$  if  $\pi_{\text{red}} = \{\mathcal{N}_a, \mathcal{N}_b\}$  is an A.E.P. of the **reduced graph**  $\mathcal{G}_{\text{red}}$ .

$\implies$  Relationship to original graph  $\mathcal{G}$ ?

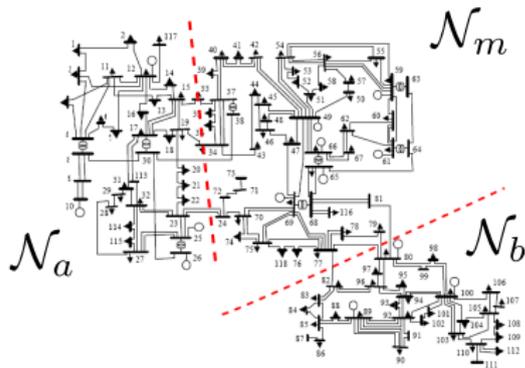
# Kron Reduction & Almost Equitable Partitions

## Proposition

$\pi = \{\mathcal{N}_a, \mathcal{N}_m, \mathcal{N}_b\}$   
is an A.E.P. of  $\mathcal{G}$

↓

$\pi_{\text{red}} = \{\mathcal{N}_a, \mathcal{N}_b\}$   
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⇒ A.E.P. preserved under Kron Reduction

$$v_{\text{area}} = \mu_a - \mu_b \quad \text{if} \quad \{\mathcal{N}_a, \mathcal{N}_m, \mathcal{N}_b\} \text{ is an A.E.P.}$$

⇒ Calculate  $v_{\text{area}}$  from **pure voltage measurements**

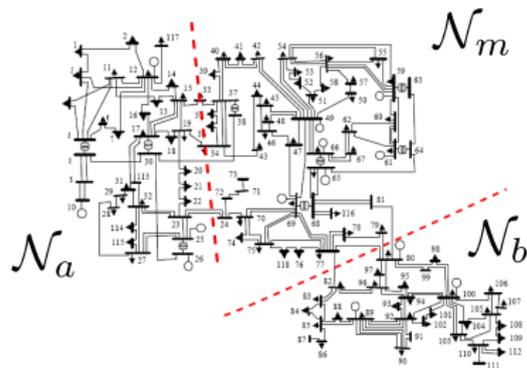
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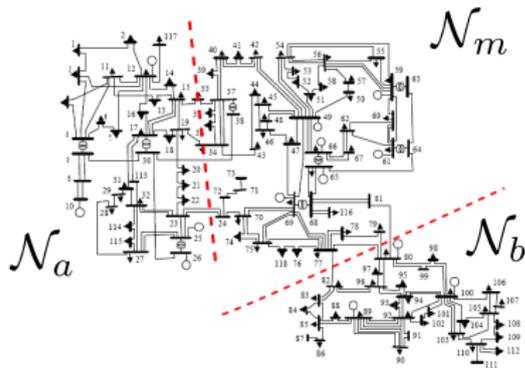
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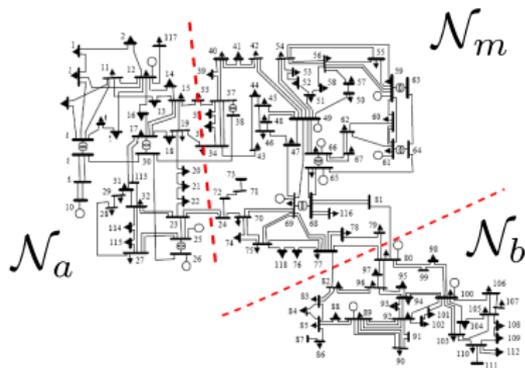
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# Conclusions

Theoretical development for **cutset and area voltage**:

- 1  $v_{\text{cut}} = (\text{diff. in mean voltage levels}) + \text{remainder } \varepsilon_{\text{cut}}$
- 2 Remainder vanishes for almost equitable partitions
- 3 Also holds for voltage across area
- 4 Kron Reduction preserves A.E.P.

## Open Problems:

- 1 Optimal cutset selection, “spanning cutsets”
- 2 Refine treatment of border buses
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`https://ece.uwaterloo.ca/~jwsimpso/  
jwsimpson@uwaterloo.ca`

**appendix**

# The Optimal Frequency Regulation Problem

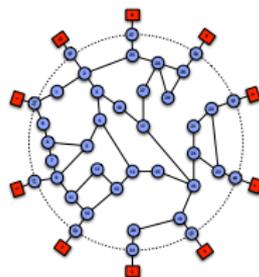
(Simplified, Linearized, and Network-Reduced)

**Grid:**  $\mathcal{G} = (\mathcal{V}, \mathcal{E}, B)$

Swing Dynamics

$$\dot{\theta}_i = \omega_i$$

$$M_i \dot{\omega}_i = -D_i \omega_i + P_i^* - P_{e,i}(\theta) + p_i$$



(Linearized) Power Flow

$$P_{e,i}(\theta) = \sum_{j=1}^n B_{ij}(\theta_i - \theta_j),$$

**Problem:** How to pick controls  $p_i$   
for (i)  $\omega_{ss} = 0$  (ii) optimality?

OFR Problem

$$\text{minimize}_{p \in \mathbb{R}^n} \sum_{i=1}^n \frac{1}{2} k_i p_i^2$$

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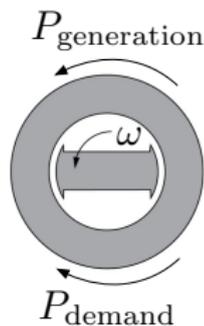
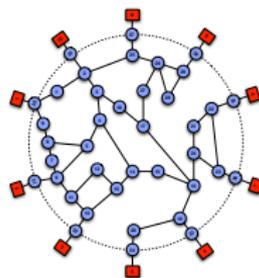
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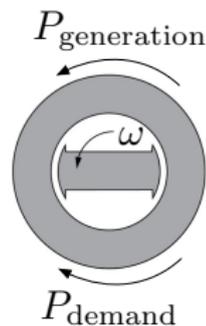
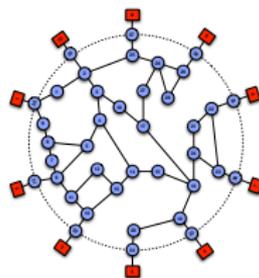
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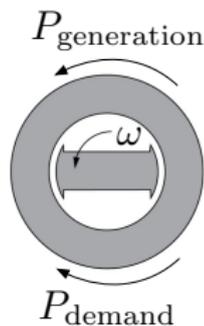
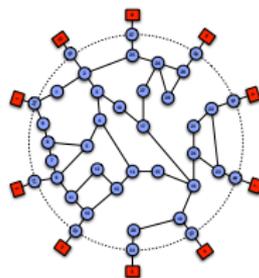
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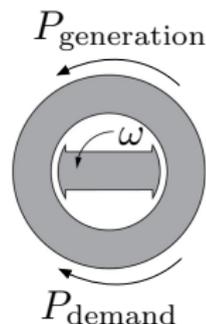
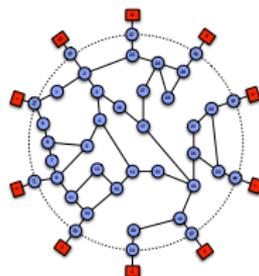
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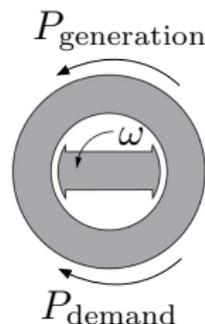
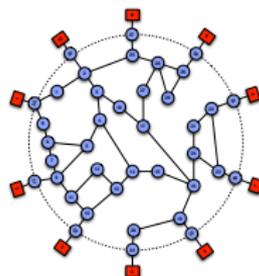
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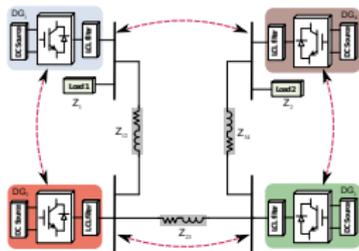
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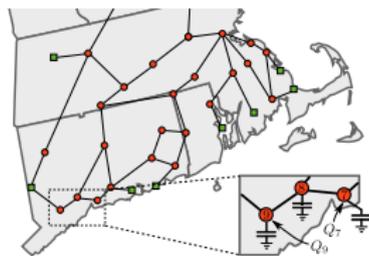
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# Smart Grid Project Samples

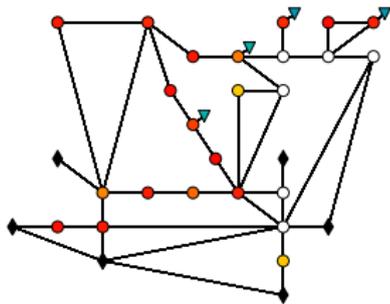
## Distributed Inverter Control



## Voltage Collapse (Nat. Comms.)



## Optimal Distrib. Volt/Var (CDC)



## Wide-Area Monitoring (TSG)

