

A Theory of Solvability for Lossless Power Flow Equations

John W. Simpson-Porco



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1361


A Theory of Solvability for Lossless Power Flow Equations—Part I: Fixed-Point Power Flow

John W. Simpson-Porco , *Member, IEEE*

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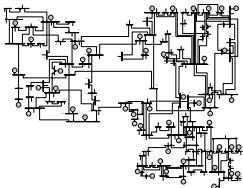
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A Theory of Solvability for Lossless Power Flow Equations—Part II: Conditions for Radial Networks

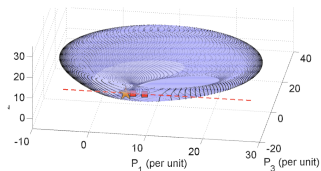
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Problems in power system operations

Power Flow Analysis

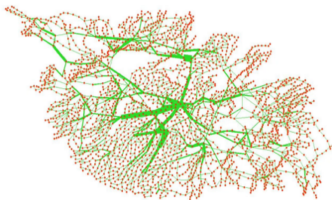


Optimal Power Flow



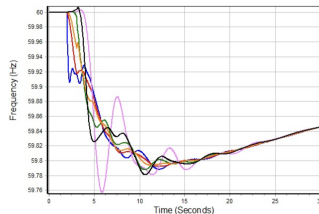
[Molzahn et al.]

Contingency Analysis



[Rezaei et al.]

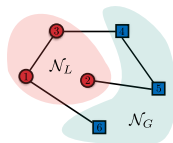
Transient Stability



[Overbye et al.]

Modeling AC power flow

- active power: $P_i = \sum_j V_i V_j B_{ij} \sin(\theta_i - \theta_j)$
- reactive power: $Q_i = -\sum_j V_i V_j B_{ij} \cos(\theta_i - \theta_j)$



⑥ n Loads (●) and m Generators (■) $\mathcal{N} = \mathcal{N}_L \cup \mathcal{N}_G$

⑦ **Load Model:** PQ bus constant P_i constant Q_i

⑧ **Generator Model:** PV bus constant P_i constant V_i ,

Power Flow Equations

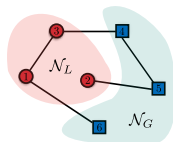
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$2n + m$ equations in variables $\theta \in \mathbb{T}^{n+m}$ and $V_L \in \mathbb{R}_{>0}^n$.

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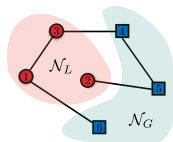
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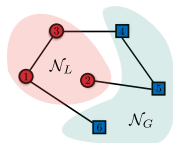
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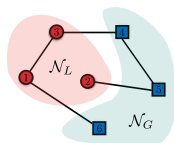
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Why study solvability of power flow problems?

① Because it is interesting to do so

② Numerical methods

- understand convergence, divergence, and initialization issues

- **State vector:** $x = (\theta, V_L)$

- **Newton iteration:**

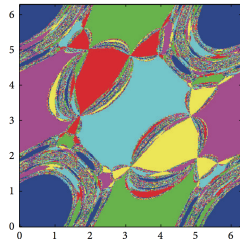
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③ Optimal power flow

④ Transient stability



[Deng et al.]

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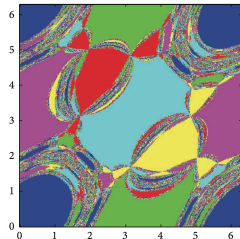
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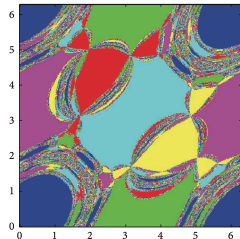
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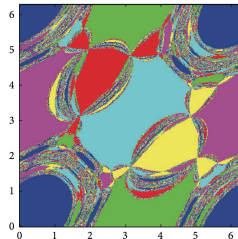
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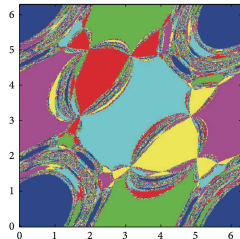
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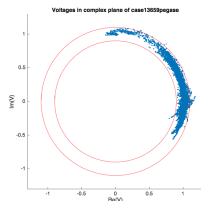
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Intuition on power flow solutions

① 'Normally', exists unique **high-voltage** soln:

- voltage magnitude $V_i \simeq 1$
- phase diff $|\theta_i - \theta_j| \ll 1$



[Josz et al.]

② **Lightly loaded systems:** many **low-voltage** solutions

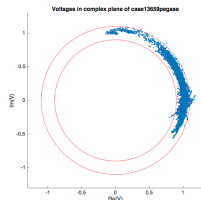
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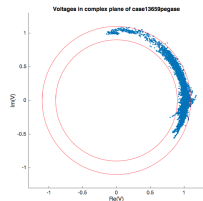
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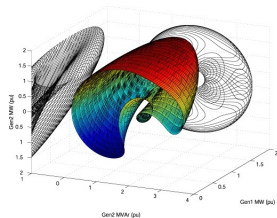


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[Hiskens & Davy]

Mysteries of power flow

Given data: network topology, impedances, generation & loads

Q: \exists “stable high-voltage” solution? unique? properties?

Partial answers from **45+ years** of literature:

- Jacobian singularity [Weedy '67]
- Multiple dynamically stable solutions [Korsak '72]
- Existence conditions [Wu & Kumagai '80, '82]
- Active power flow singularity [Araposthatis, Sastry & Varaiya, '81]
- Counting # of solutions [Baillieul and Byrnes '82]
- Properties of quadratic equations [Makarov, Hill & Hiskens '00]
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- Existence/uniqueness for active power flow [Dörfler, Chertkov & Bullo '12, Delabays, Coletta, and Jacquod '17, JWSP '17, Jafarpour and Bullo '18]
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- Existence/uniqueness in distribution networks [Bolognani & Zampieri '16, Nguyen *et al.* '17, Wang *et al.* '17, Bazrafshan *et al.* '17, ...]

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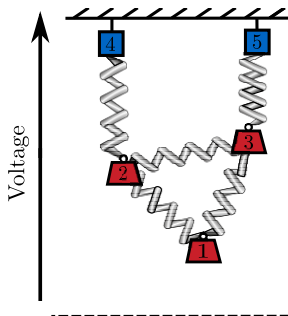
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Main insight: stiffness vs. loading

- 1 Stiff network + light loading \Rightarrow feasible
- 2 Weak network + heavy loading \Rightarrow infeasible

Q: How to quantify network stiffness vs. loading?



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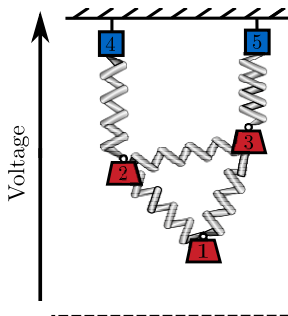
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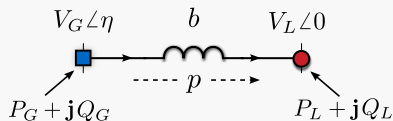


Solution of Two-Bus System I

$$P_L = bV_G V_L \sin(-\eta)$$

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① Lossless Network $\implies P_G = -P_L = p$

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② Eliminate η

$$p^2 + (Q_L - bV_L^2)^2 = b^2 V_G^2 V_L^2,$$

③ Change Variables

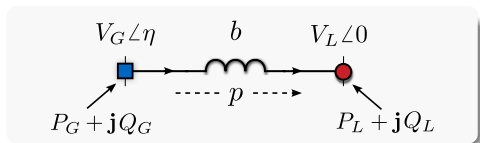
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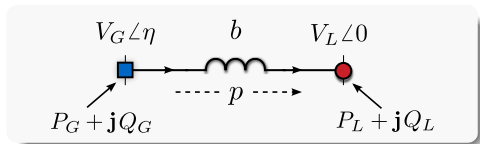
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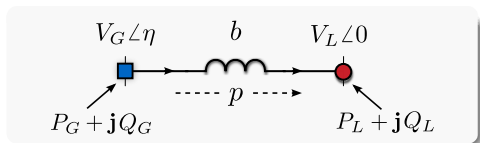
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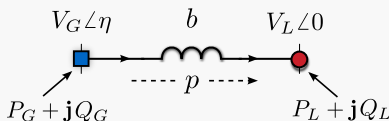
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Solution of Two-Bus System II

$$p = bV_G V_L \sin(\eta)$$
$$Q_L = bV_L^2 - bV_L V_G \cos(\eta)$$



3 Change Variables

$$v := \frac{V_L}{V_G} \quad \Gamma := \frac{p}{bV_G^2} \quad \Delta := \frac{Q_L}{-\frac{1}{4}bV_G^2}$$

4 Solve Quadratic in v^2

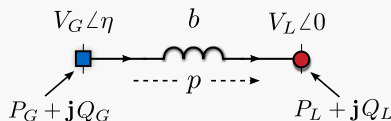
$$v_{\pm} = \sqrt{\frac{1}{2} \left(1 - \frac{\Delta}{2} \pm \sqrt{1 - (4\Gamma^2 + \Delta)} \right)}$$

5 Nec. & Suff. Condition

$$4\Gamma^2 + \Delta < 1$$

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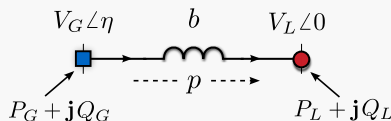
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Solution of Two-Bus System III

$$\Gamma = v \sin(\eta)$$

$$\Delta = -4v^2 + 4v \cos(\eta)$$

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- ① **High-voltage** solution

$$v_+ \in [\frac{1}{2}, 1)$$

- ② **Low-voltage** solution

$$v_- \in [0, \frac{1}{\sqrt{2}})$$

Angle: $\sin(\eta_{\mp}) = \Gamma/v_{\pm}$

- ① **Small-angle** solution

$$\eta_- \in [0, \pi/4)$$

- ② **Large-angle** solution

$$\eta_+ \in [0, \pi/2)$$

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$$v_+ \in [\frac{1}{2}, 1)$$

- ② **Low-voltage** solution

$$v_- \in [0, \frac{1}{\sqrt{2}})$$

Angle: $\sin(\eta_{\mp}) = \Gamma/v_{\pm}$

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Solution of Two-Bus System III

$$\Gamma = v \sin(\eta)$$

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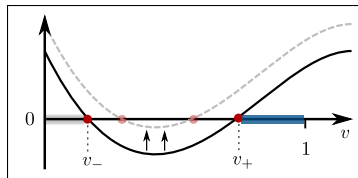
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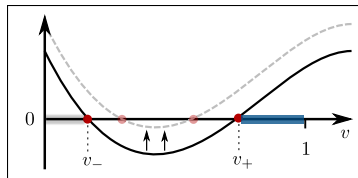
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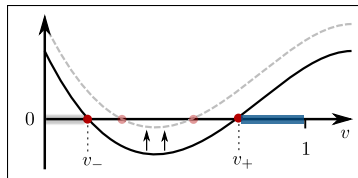
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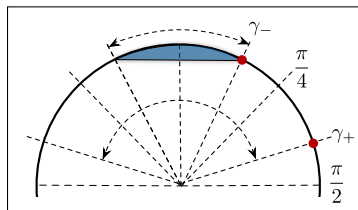
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Solution of Two-Bus System IV

- Squaring and adding equations **does not generalize** to networks.
- Is there any hope then?

$$\Gamma = v \sin(\eta)$$

$$\Delta = -4v^2 + 4v \cos(\eta)$$

- Use $\cos(\eta) = \sqrt{1 - \sin^2(\eta)} \implies \Delta = -4v^2 + 4v\sqrt{1 - (\Gamma/v)^2}$
- Rearrange to get *fixed-point equation*

$$v = f(v) := -\frac{1}{4} \frac{\Delta}{v} + \sqrt{1 - \left(\frac{\Gamma}{v}\right)^2}$$

This generalizes!

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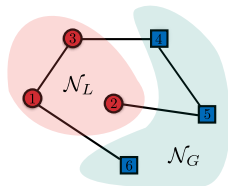
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Network Notation I: Branches Between Bus Types

Power Flow Equations

$$P_i = \sum_j V_i V_j B_{ij} \sin(\theta_i - \theta_j), \quad i \in \mathcal{N}_L \cup \mathcal{N}_G$$

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- Bus partitioning $\mathcal{N} = \mathcal{N}_L \cup \mathcal{N}_G$ induces **branch partitioning**

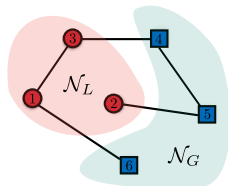
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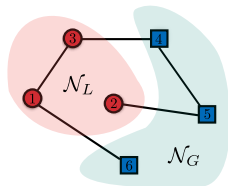
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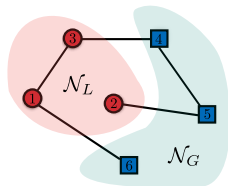
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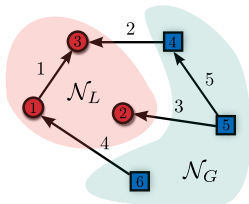
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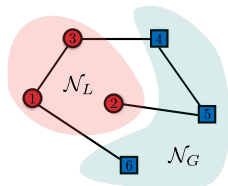
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- **Generators** \mathcal{N}_G : V_i fixed
- **Loads** \mathcal{N}_L : V_i free



Partitioned Variables

$$V = \begin{pmatrix} V_L \\ V_G \end{pmatrix}, \quad B = \begin{pmatrix} B_{LL} & B_{LG} \\ B_{GL} & B_{GG} \end{pmatrix}$$

Open-circuit voltages

$$V_L^* \triangleq \underbrace{-B_{LL}^{-1} B_{LG}}_{\text{Generators} \rightarrow \text{Loads}} \cdot V_G$$

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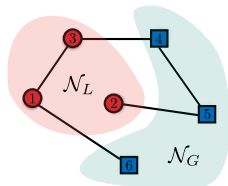
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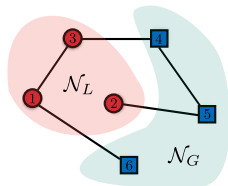
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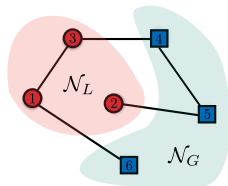
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- Need to **non-dimensionalize** power flow equations
- **Stiffness matrices** quantify **grid strength** in **units of power**

① **Nodal** stiffness matrix

$$S \triangleq \frac{1}{4} [V_L^*] \cdot B_{LL} \cdot [V_L^*]$$

② **Branch** stiffness matrix

$$D \triangleq [V_i^* V_j^* B_{ij}]_{(i,j) \in \mathcal{E}}$$

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Main Modeling Result

Fixed-Point Power Flow: Meshed Networks

(θ, V_L) is a power flow solution iff (v, p_c) solves the FPPF

$$v = f(v, p_c) \triangleq \mathbb{1}_n - \frac{1}{4} S^{-1} [Q_L] [v]^{-1} \mathbb{1}_n \\ + \frac{1}{4} S^{-1} [v]^{-1} |A|_L D [h(v)] u(v, p_c),$$

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$$\mathbb{0}_c = \mathbf{C}^T \mathbf{arcsin}(\psi(v, p_c)).$$

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with the phase angles $\mathbf{A}^T \theta = \mathbf{arcsin}(\psi)$.

New Approximate Power Flow Solution

- The model says $v = f(v, p_c)$, and $\sin(A^T \theta) = \psi(v, p_c)$.
- By construction, when $P = Q_L = 0$, a solution is

$$v = \mathbf{1}_n, \quad p_c = 0_c, \quad A^T \theta = 0_{|\mathcal{E}|}.$$

- **Taylor expand** FPPF model around this solution

$$A^T \theta_{\text{approx}} = A^T L^\dagger P$$

$$v_{\text{approx}} \simeq \mathbf{1}_n - \frac{1}{4} S^{-1} Q_L + \frac{1}{8} S^{-1} |A|_L D[A^T L^\dagger P] A^T L^\dagger P$$

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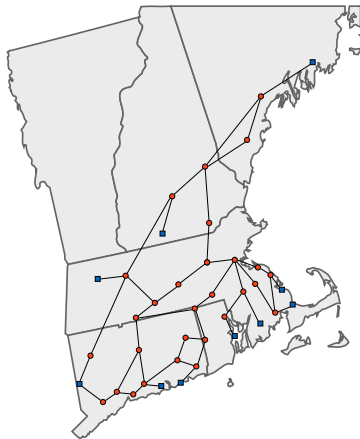
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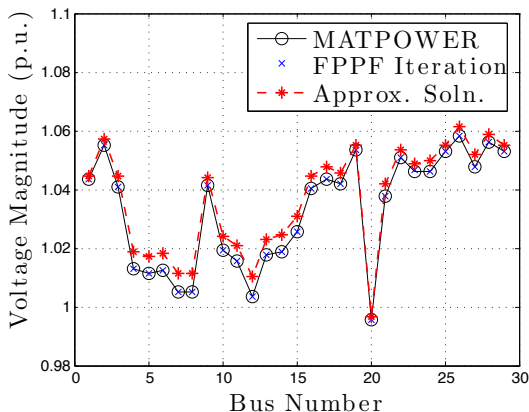
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Numerical Results

$$\delta_{\max} = \|v - v_{\text{approx}}\|_{\infty}, \quad \delta_{\text{avg}} = \frac{1}{n} \|v - v_{\text{approx}}\|_1$$

	Base Load			High Load	
Test Case	FPPF Iters.	δ_{\max} (p.u.)	δ_{avg} (p.u.)	FPPF Iters.	δ_{\max} (p.u.)
New England 39	4	0.006	0.004	8	0.086
57 bus system	5	0.011	0.003	8	0.118
RTS '96 (3 area)	4	0.003	0.001	8	0.084
118 bus system	3	0.001	0.000	7	0.054
300 bus system	6	0.022	0.004	8	0.059
PEGASE 1,354	5	0.011	0.001	8	0.070
Polish 2,383 wp	4	0.003	0.000	8	0.078
PEGASE 2,869	5	0.015	0.002	8	0.098
PEGASE 9,241	6	0.063	0.003	9	0.133

FPPF Simplifies for Acyclic Networks

Fixed-Point Power Flow: Radial Networks

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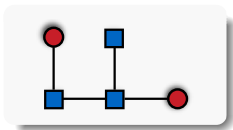
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On what invariant set is f a **contraction**?

Solvability Results for Different Acyclic Topologies

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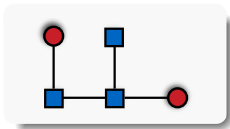
PQ buses have one PV bus neighbor



Sufficient + Necessary
Existence + Uniqueness

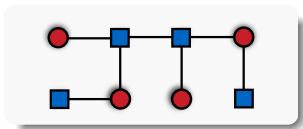
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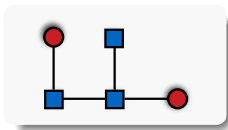
PQ buses have many PV bus neighbors



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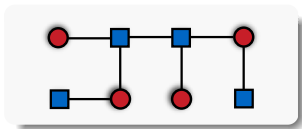
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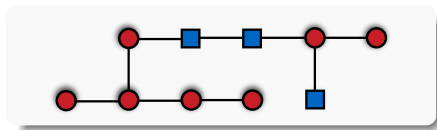
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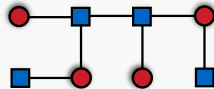
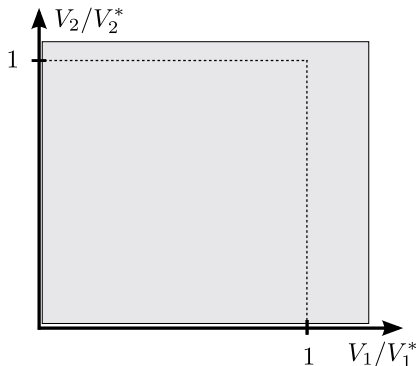
Sufficient + Tight
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General interconnections



Sufficient
Existence

Partitioning of Voltage Space



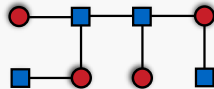
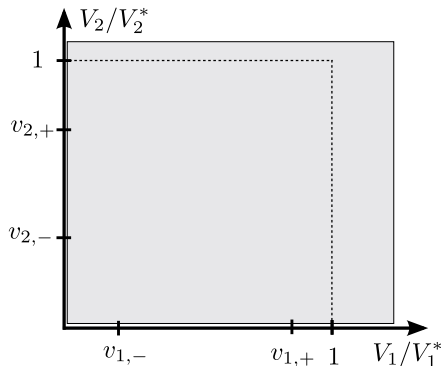
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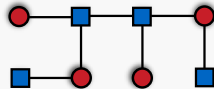
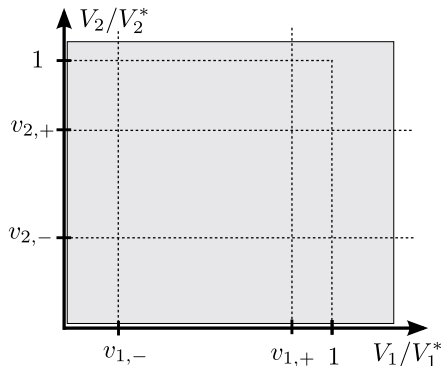
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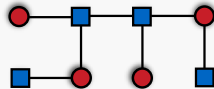
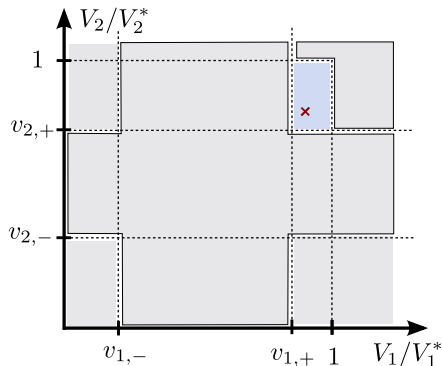
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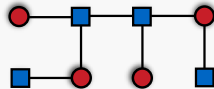
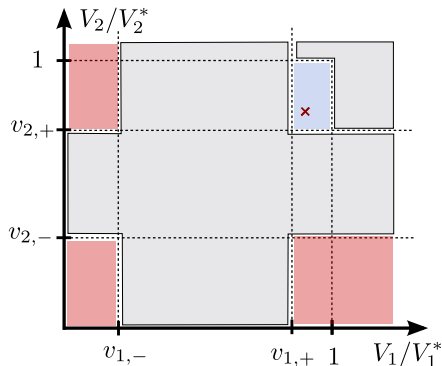
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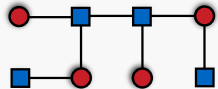
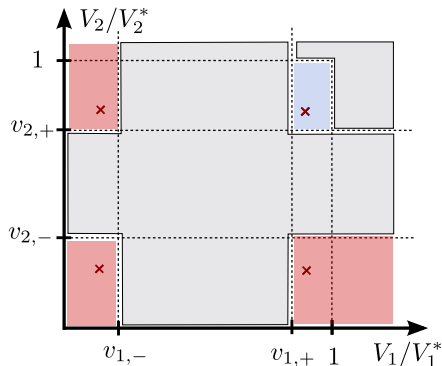
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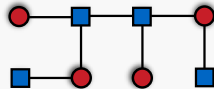
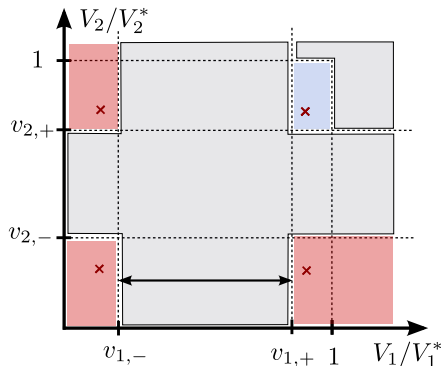
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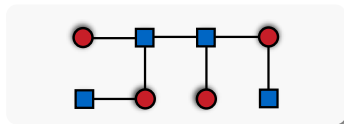
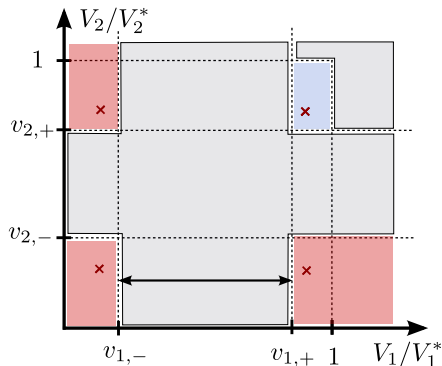
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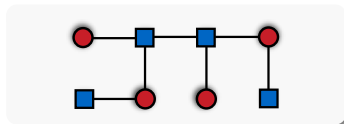
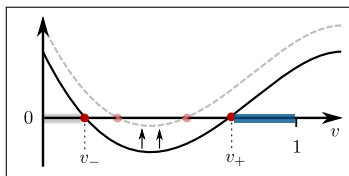
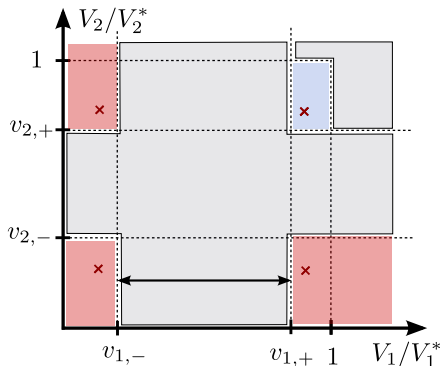
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- 2 Approximate solution

A Theory of Solvability for Lossless Power Flow
Equations — Part I: Fixed-Point Power Flow

John W. Simpson-Porco, *Member, IEEE*

New **conditions for power flow solvability**:

- 3 Contractive iteration
- 4 Existence/uniqueness
- 5 Generalizes known results

What's next?

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- 2 **Lossy** networks (TPWRS: JWSP '17)
- 3 Applications ($n - 1$, opt/control)

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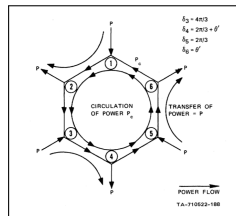
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Questions



<https://ece.uwaterloo.ca/~jwsimpso/>
jwsimpson@uwaterloo.ca

appendix

Power flow and grid connectivity

*"[Power flow feasibility] is one question which is unresolved in power systems analysis, but which is of basic theoretical and practical importance . . . **is a given network structurally susceptible to unfeasibility?** What type and what value of injections are most likely to result in unfeasible situations?"*

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*"The power systems theory needs to be pushed further in the direction of exploiting **structural features of the networks** . . . realistic power systems models have at least two different types of node dynamics (generators, loads) and the directional power flows between them play a major role."*

— D. J. Hill & G. Chen, 2006

*"**Root causes of [the northeastern] blackout: lack of basic understanding of power systems . . . theoretical understanding of nonlinear power system dynamics is inadequate.** It is time for more theoretical research to develop alternatives to complement scenario-based simulation paradigm: mathematical theory to understand the complex dynamic behavior of large-scale interconnected power systems utilizing modern nonlinear mathematics."*

— Felix F. Wu, 2003

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Power flow and grid connectivity

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